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bubble surface effect ship XR-3 digital
computer loads and motion program

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A STUDY OF PRESSURE-VOLUME RATES AND PLENUM
MEMBRANE ADDITIONS TO THE CAPTURED AIR
BUBBLE SURFACE EFFECT SHIP XR-3 DIGITAL
COMPUTER LOADS AND MOTION PROGRAM

John Martin Boggio

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

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AIR BUBBLE SURFACE EFFECT SHIP XR-3
DIGITAL COMPUTER LOADS AND MOTION PROGRAM

by

John Martin Boggio

June 1976

Thesis Advisor:

A. Gerba, Jr.

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A Study of Pressure-Volume Rates and Plenum
Membrane Additions to the Captured Air
Bubble Surface Effect Ship XR-3 Digital
Computer Loads and Motion Program

by

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Lieutenant, United States Navy
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Submitted in partial fulfillment of the
requirements for the degree of

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June 1976

ABSTRACT

A study was conducted of modeling changes to the XR-3 Captured Air Bubble Surface Effect Ship digital computer Loads and Motion program. These changes included the addition of pressure rate and volume rate to the existing 6 degrees of freedom equations. Additional equations were developed to simulate the application of a nonpermeable membrane to the plenum of the XR-3 test craft. The objectives of this study were to determine whether the addition of pressure rate and volume rate equations would improve computer execution time and to test some simplified models of the plenum membrane. Computer timing improvements were demonstrated and membrane modeling results are presented.

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I. INTRODUCTION

A. BACKGROUND

The Captured Air Bubble Surface Effect Ship (CAB SES) offers a dynamic new approach to improve surface ship performance. As with any new approach, extensive testing at the design stage of development is required. The U.S. Navy has been conducting sea trials on two 100 ton Captured Air Bubble (CAB) test craft, the 100-A and the 100-B [Ref. 1]. In addition to scale model testing, another approach to design evaluation involves the use of high speed digital computers to simulate the dynamic performance of the craft.

A digital computer Loads and Motion (L&M) program for the CAB SES was developed under government contract by the Oceanics Corp. [Ref. 2]. The L&M program installed at the Naval Postgraduate School, W. R. Church, computer facility on an IBM 360/67 computer was for a 100 ton displacement test craft, the 100-B. Leo and Boncal [Ref. 3] modified this computer program to represent a smaller 3 ton craft, the XR-3. The XR-3 is an operational test craft currently maintained and operated by the Naval Postgraduate School [Ref. 4].

Various modifications and changes to Leo and Boncal's basic work have been implemented. Finley, Forbes, and Menzel, in Refs. 5-7, provides program changes to obtain better representation of the Fan maps, bow and stern seal dynamics and pitch and roll damping.

One adverse characteristic of both the 100-B computer program and the XR-3 computer program was the extensive use of the digital computer time when operating in simulated sea states. Since the 100-B and the XR-3 programs are similiar, the computer time analysis provided by Mitchell [Ref. 8] for the 100-B also applies to the XR-3 program.

Another aid to design is the testing done in towing tanks in which scale models are used. Towing tests were conducted at NSRDC using a rubber membrane installed on the forward portion of a CAB SES model in order to better scale the pressure-volume relationship [Ref. 9]. The addition of this membrane improved the pitch and heave characteristics of the scale model in sea state operation.

B. OBJECTIVES

It is the objective of this work to examine the L&M digital computer program and make any changes that would improve the program with particular attention to changes that would reduce the amount of time required to execute the program.

A second objective is to model the plenum membrane, add the required program changes and study the effects of the membrane on simulated craft performance.

II. PROGRAMMING CHANGES

A. RATE EQUATIONS FOR PRESSURE AND VOLUME

1. Introduction

An examination of the dynamics of the XR-3 L&M program indicate that the key parameters of this type of ship design are those which describe the dynamic behavior of the bubble of the air in the plenum. This pressure of air provides approximately 75% of the lift force when the craft is "on the bubble." Small changes in bubble volume and pressure therefore cause significant changes in total ship response. These variables were examined in an effort to decrease the digital computer simulation execution time.

2. SUBROUTINES RHS and INTGRL

The force and moment equations for the craft are the six degrees of freedom equations plus four auxillary equations contained in SUBROUTINE RHS [Ref. 2].

The integration of these equations is performed in SUBROUTINE INTGRL. INTGRL uses the Runge-Kutta-Merson numerical integration technique with an automatic variable step size. If the error tolerances specified are exceeded the step size is reduced and the step repeated until all error tolerances are met or the step size is reduced to 1×10^{-6} sec., at which point the program stops. Thus the integration values are forced to converge to their correct values. All ten equations are integrated serially at the

same time step. When all integration error tolerances are met INTGRL returns the integrated values and increases the simulation time one time-step increment. Since pressure and volume are key variables, integrating their rates should cause the system of equations to converge more rapidly to their true values and avoid any problems associated with the feedback loops in the pressure-volume calculation [Ref. 10].

3. Formulation of Volume Rate and Pressure Rate

The bubble pressure equation is for an adiabatic process [Ref. 2].

$$P_b = P_a \left(\frac{\rho_b}{\rho_a} \right)^\gamma \quad (1)$$

where the subscripts a and b represent atmosphere and plenum values respectively

P = pressure absolute

$$\rho = \text{density } \frac{M}{V} \quad (2)$$

γ = adiabatic exponent for air

Substituting (2) into (1)

$$P_b = P_a \left(\frac{M}{V \rho_a} \right)^\gamma \quad (3)$$

Differentiating (3) with respect to time where P_a and ρ_a are assumed to be constant yields

$$\dot{P}_b = \frac{P_a}{\rho_a} \gamma \left(\frac{M}{V \rho_a} \right)^{\gamma-1} \left(\frac{\dot{VM} - M\dot{V}}{V^2} \right) \quad (4)$$

Factoring $\frac{M}{V}$ from the last term of (4)

$$\dot{P}_b = \gamma P_a \left(\frac{M}{\rho_a V} \right)^{\gamma-1} \left(\frac{M}{\rho_a V} \right) \left(\frac{\dot{M}}{M} - \frac{\dot{V}}{V} \right) \quad (5)$$

Noting $\left(\frac{M}{\rho_a V} \right)^{\gamma-1} \left(\frac{M}{\rho_a V} \right) = \left(\frac{M}{\rho_a V} \right)^{\gamma}$

and

$$P_a \left(\frac{M}{\rho_a V} \right)^{\gamma} = P_b$$

$$\dot{P}_b = \gamma P_b \left(\frac{\dot{M}}{M} - \frac{\dot{V}}{V} \right) \quad (6)$$

The volume equation for the bubble is computed in RHS in four parts and summed together

$$V = V_{nom} - D - WA + WT \quad (7)$$

The four terms that determine volume are

- (1) V_{nom} = the empty plenum volume
- (2) D = draft term-change in volume due to draft
- (3) WA = Wave term-change in volume due to the presence of waves
- (4) WT = WATSLP term-- correction term for the added volume wedge which is a function of speed [Ref. 6].

Differentiating equation (4)

$$\dot{V} = -\dot{D} - \dot{WA} \quad (8)$$

where

$\dot{W}A$ = rate of change of volume due to waves
 \dot{D} = rate of change of volume due to displacement
 $\dot{W}T$ = 0.0
 $\dot{V}nom$ = 0.0

$\dot{W}A$ is computed in SUBROUTINE WAVES by taking the difference in change of volume due to waves at successive time steps and dividing by the time step. Since WATSLP is a function of speed, the differentiated value of WATSLP, $\dot{W}T$, is a function of acceleration. Forward accelerations are normally small; therefore, the differentiated value of WATSLP was approximated to be zero. Equations (4) and (5) were programmed as follows:

VALUE (11) = -(((XL*WIDTH)-ABW)*.5*W)-DVWDOT
VALUE (12) = GAM*VAL(13)*(VALUE(10)/VAL(11)-VALUE(11)/
VAL(12))

where

DVWDOT = rate of change of volume due to waves
VALUE(10) = Bubble mass flow rate
VALUE(11) = Volume rate
VALUE(12) = Pressure rate
VAL(11) = Bubble Mass
VAL(12) = Bubble Volume
VAL(13) = Bubble Pressure
GAM = Adiabatic Exponent for air

B. ELIMINATION OF SUBROUTINE DMINV

In an effort to improve program timing, the suggestions given in Ref. 7 were undertaken. One recommendation suggested the removal of SUBROUTINE DMINV in the 100B L&M program by making changes to SUBROUTINES INCON and RHS. An examination of the L&M program indicated that these changes also could be applied to the XR-3 program. Consequently the following was deleted:

```
212  DO 211 I = 1,6
      DO 211 N = 1,6
211  A(I,N) = 0.0
      DO 213 N = 1,3
213  A(N,N) = AM
      A(4,4) = AIXX
      A(5,5) = AIYY
      A(6,6) = AIZZ
      A(4,6) = -AIXZ
      A(6,4) = -AIXZ
      AIMAX = AMAXI(AM, AIXX,AIYY,AIZZ,ABS(AIXZ))
      DO 214 I = 1,6
      DO 214 J = 1,6
214  A(I,J) = A(I,J)/AIMAX
      CALL DMINV(A,G,D,)
      DO 215I = 1,6
215  A(I,J) = A(I,J)/AIMAX
      IF (D.NE.0.0.) GO TO 10
      WRITE (6,216)
      STOP
```

In place of the above the following was added:

```
215  AMASSI = 1.0/AM
      D      = 1.0/(AIXX*AIZZ-AIXZ*AIXZ)
      DIXX   = AIXX*D
      DIXZ   = AIZZ*D
      DIZZ   = AIZZ*D
      AIYYI  = 1.0/AIYY
      GO TO 10
```

Linkage between INCON and RHS was provided by the following

```
COMMON/ATRIX/AMASSI,AIYYI,DIXX,DIXZ,DIZZ
```

In SUBROUTINE RHS the six element matrix GF(J) was deleted and the following identifiers were substituted for the summation of forces: SUMX, SUMY, SUMZ, SUMK, SUMM, SUMN. In addition, the following deletion was made.

```
DO 1 I = 1,6
VALUE(I) = 0.0
DO 1 J = 1,6
VALUE (I) = VALUE (I) + A(I,J)*GF(J)
1 CONTINUE
```

Substituted for the above DO LOOPS was the following

```
VALUE (1)  = SUMX*AMASSI
VALUE (2)  = SUMY*AMASSI -R*U
VALUE (3)  = SUMZ*AMASSI
VALUE (4)  = SUMK*DIZZ + SUMN*DIXZ
```

VALUE (5) = SUMM*AIYYI

VALUE (6) = SUMN*DIXX + SUMK*DIXZ

These changes eliminated SUBROUTINE DMINV and several DO LOOPS.

C. EXPANSION OF WAVE COMPONENTS

Since the program was being tested with sea state, the method used for the wave generation was studied. SUBROUTINE INCON provides a means of introducing sea-state by individual wave components and amplitudes. In addition, the subroutine will accept an average height and lowest and highest wave frequency and/or wave period and generate up to 10 wave components.

These wave components represent a sampling of the spectral energy density of the given sea state condition. Reference 11 suggests for irregular sea, a minimum of 15 - 20 components are required to simulate irregular sea conditions. The program dimension statements were accordingly increased from 10-20 to determine if any significant changes could be observed by increasing the number of wave components.

D. MISCELLANEOUS

Each subroutine was examined with regard to efficiency of coding and changes were implemented such as multiplication in lieu of the use of the exponential. For example, IBM 360/67 fixed point exponentiation requires that the natural logarithm be generated and then a logarithm be computed, as compared

to straight forward multiplication. When such exponentiation is nested in DO LOOPS, a significant time savings can be realized by the use of multiplication.

III. TEST PRODECURES

A. COMPUTER SYSTEM

The digital computer used throughout this study is an IBM 360/67 model, VERSION I, located at the NPS W. R. Church Computer Facility. The system's hardware configuration provides 2 M bytes of core. This main core is composed of IBM core storage devices (IBM 2365 Mod. 12) and compatable but slightly different Lockheed core storage devices (MM 365). The Lockheed core devices are about 18% slower in execution time than IBM core devices. Since the system is time-shared and the core is contiguous, there is no practical way to determine in which portion of the main core the program is residing. Therefore, exact timing of a program is not easily achieved. In this report all timing values must be interpreted with this anomaly in mind. Among the options available under this operating system are the FORTRAM G and FORTRAN H compilers [Ref. 12]. Mitchell reported substantial time savings using the H compiler [Ref. 8]. Since one of the main objectives was to reduce execution time, computer model testing was done using both compiler options. Runs made under different compilers will be noted.

A word of caution on the use of the H compiler. The H compiler produces its timing improvements and core reduction by coding optimization. This means the compiler re-arranges

the Fortran code. This re-arrangement may move computations outside of DO LOOPS for example. Applicable portions of Ref. 13 should be read and understood before using this feature.

B. TEST CONDITIONS

The L&M program for the XR-3 used in this report is the one given in Ref. 7. This program was then modified to incorporate the changes previously described. The basic program [Ref. 7] computes pressure using eq. (1) and volume using eq. (7) and is referred to as PROGRAM ONE. PROGRAM ONE was used as reference for comparative purposes. The addition of the pressure rate and volume rate equations (6) and (8) and the elimination of SUBROUTINE DMINV constituted major modifications to the basic program. This version of the Loads and Motion program was called PROGRAM TWO. PROGRAM THREE was PROGRAM TWO compiled and executed with the FORTRAN H compiler.

Five test conditions for a given speed were established to provide a full range of disturbances for testing the L&M programs. These test conditions are tabulated in Table I.

In Condition One small disturbances were introduced by changing the initial conditions of draft (DS) and pitch (θ). These changes consisted of decreasing the draft and pitch from previously computed steady state values by the magnitude shown in Table I. In addition, the rudder was held at zero and the sea was calm. In Condition Two, the perturbations were the same as Condition One except that now the rudder

TABLE I

TEST PERTURBATIONS

	ΔDS	$\Delta \theta$	RUDDER	SEA STATE
Condition One	0.1 inch	.03	0.0	Calm water
Condition Two	0.1	.03	20°	Calm water
Condition Three	0.0	0.0	0.0	Regular One
Condition Four	0.0	0.0	0.0	Regular Two
Condition Five	0.0	0.0	0.0	Irregular One

was displaced to the right 20 degrees. The rudder was offset at the start of the simulation and held through the run as this value. In Condition Three, Four and Five the only disturbances used were the sea state conditions.

Sea state is generated in SUBROUTINE WAVES. SUBROUTINE INCON generates wave components and amplitudes based on several different type input parameters. [See users manual Ref. 7]. Regular sea one and two are simple sinusoidal waves. Irregular sea state conditions are simulated by the addition of several regular sinusoidal wave components. Sea state used throughout this study is true sea state and is not scaled in any manner.

The L&M program provides two options for propulsion, either constant speed or constant thrust. The constant

thrust option was selected because this is the normal operating mode for the XR-3 test craft.

Integrator tolerance levels were maintained at the values given in Ref. 7. However two new error tolerances had to be determined for the integration of the pressure and volume rates. These new levels were determined by first selecting a very tight value .000001 which was increased in increments until a change in output could be noticed. The value was then decreased by a factor of 10. Pressure and volume tolerance levels were then set at this value which was found to be .0001.

All other variables such as draft, and pressure were initialized from the steady state undisturbed conditions for that specific starting speed. The steady state conditions were evaluated by first using the constant speed propulsion option and the initial values in Ref. 7. The program was then run until the key input variables - pitch, draft, thrust and pressure - reached steady state. These values were then read in and propulsion was switched to constant thrust. The program was run again to insure that steady state conditions existed. These steady state values are shown in Table II.

TABLE II

STEADY STATE CONDITIONS

Speed(Knots)	10	20	30
Pressure	23.93	24.84	24.84
Draft	8.17	6.12	5.34
Thrust (each engine)	200.31	218.17	287.22
Pitch	1.62	.48	.26

Pressure in psfg

Thrust in ft. lb.

Draft in inches

Pitch in degrees

IV. MEMBRANE ADDITION

A. INTRODUCTION

During towing tank tests conducted at NSRDC, a rubber membrane was installed on the forward bow of the XR-1 scale model [Ref. 9]. The installation of this membrane improved the pitch and heave characteristics of the scale model during simulated sea conditions. Reference 9 provided the following empirical expression which relates the Pressure and Volume of the membrane.

$$V = KP_b \quad (9)$$

K was experimentally determined and has the value .317 when scaled to the XR-3 test craft dimensions. (See Appendix A).

B. MATHEMATICAL MODELING

The approach used to include the effects of this membrane was to develop mathematical expressions which could be added to the already existing pressure, volume and air mass equations in the L&M program. Five mathematical expressions were developed, tested and referred to as Models One, Two, Three, Four and Five. They are explained below and the results discussed in Section V.

1. Model One

Model One is based on the premise that by correcting the plenum volume with the membrane volume, the equations

in SUBROUTINE RHS would show the effect of the membrane.

Model One added the following equation to PROGRAM ONE;

$$V_m = K P_m \quad (10)$$

Then using (10) to correct the volume of the plenum and assuming $P_m = P_b$.

$$V = V_b + V_m \quad (11)$$

where V_b is given by eq. (7).

2. Model Two

Model Two is an extension of Model One. Based on the premise that by correcting the rate of change of plenum volume with the rate of change of membrane volume, the rate equations given in SUBROUTINE RHS and subsequent integration of these terms would show the effect of the membrane. Model Two added the following rate equation to PROGRAM TWO.

$$\dot{V}_m = K \dot{P}_m \quad (12)$$

Then using (12) to correct the rate of change of plenum volume and assuming

$$\begin{aligned} \dot{P}_m &= \dot{P}_b \\ \dot{V} &= \dot{V}_b + \dot{V}_m \end{aligned}$$

where \dot{V}_b is given by eq. (8).

3. Model Three

Model Three was based on the premise that the volume rate eq. (8) and the pressure rate eq. (6) as computed without the membrane could be corrected for the membrane by adjusting these terms by appropriate factors within PROGRAM TWO.

Correction terms were sought that would be a function of the membrane. A logical candidate for this correction factor for the pressure was the ratio of rates of change of the membrane volume to plenum volume multiplied by plenum pressure rate.

$$PCT = \frac{\dot{V}_m}{\dot{V}_b} \dot{P}_b \quad (13)$$

where PCT is the correction factor to be added to the plenum pressure rate term \dot{P}_b before integration. It was assumed that the pressure and pressure rate of the plenum and membrane were equal.

$$P_m = P_b \quad (14)$$

$$\dot{P}_m = \dot{P}_b \quad (15)$$

It was also assumed that the membrane volume rate and pressure rate were related by

$$\dot{V}_m = K \dot{P}_m \quad (16)$$

Substituting (16) into (13) and using (15)

$$PCT = K \frac{\dot{P}_b^2}{\dot{V}_b} \quad (17)$$

The volume rate correction term was assumed to be the ratio of the rate of change of membrane pressure to the rate of change of plenum pressure times the rate of change of membrane volume.

$$VCT = \frac{\dot{P}_m}{\dot{P}_b} \dot{V}_m \quad (18)$$

where VCT is the correction factor to be added to the plenum volume rate term \dot{V}_b before integration

$$\text{Since } \dot{P}_m = \dot{P}_b \text{ and } \dot{V}_m = K\dot{P}_b$$

Then from (18)

$$VCT = K \dot{P}_b \quad (19)$$

Then using equations (17) and (19) the rate equations are

$$\dot{V} = \dot{V}_b + VCT \quad (20)$$

$$\dot{P} = \dot{P}_b + PCT \quad (21)$$

where \dot{V}_b is given by eq. (8) and \dot{P}_b by eq. (6).

Consider the following. Since K is a function of the elasticity of the membrane, if $K = 0.0$. Equations (20) and (21) reduce to the no membrane case.

If the membrane expands at the same rate that the volume of the plenum contracts the system volume rates is zero and the system pressure rate is also zero.

4. Model Four

Again using PROGRAM TWO, Model Four was based on the premise that the mass of the membrane air and mass flow rate of membrane air would be important factors in any correction term to be applied to plenum volume rate and pressure rate.

Again it was assumed that the membrane effect could be described as an adiabatic reversible process. Then using Equation (6) applied to the membrane,

$$\dot{P}_m = P_m \gamma \left(\frac{\dot{M}_m}{M_m} - \frac{\dot{V}_m}{V_m} \right) \quad (22)$$

where m denotes membrane

\dot{M}_m = Mass flow rate of the membrane air

M_m = Mass of the membrane air

Again it was assumed that the pressure and pressure rate of the membrane and plenum were equal.

$$P_m = P_b \quad (23)$$

$$\dot{P}_m = \dot{P}_b \quad (24)$$

It was also assumed that the membrane volume rate and pressure rate were related by

$$\dot{V}_m = K \dot{P}_m \quad (25)$$

Equation (25) was obtained by differentiating

$$V_m = K P_m \quad (26)$$

Substituting (25) and (26) into (22) yields

$$\frac{\dot{M}_m}{M_m} = \left(\frac{1+\gamma}{\gamma} \right) \frac{\dot{P}_m}{P_m} \quad (27)$$

One term is not available, M_m . Two possibilities were considered to determine this value. The first possibility would be to integrate \dot{M}_m and use the result of the integration from the preceding time step. The other possibility would be to hold temperatures constant in the membrane, and use the ideal gas law to determine M_m for varying pressure and volume. This last condition would be in error; however, as a first approximation, it would produce acceptable results.

Because of the past history of difficulty with integrator 10, plenum air mass rate, the second possibility was chosen. Evaluation of the terms in the ideal gas law for a temperature of 68° degrees excluding mass, pressure and volume produced the constant.

$$4.9 \times 10^{-7} \text{ slugs/psf} - \text{ft}^3$$

therefore;

$$M_m = (4.9 \times 10^{-7}) (P_m)(V_m) \quad (28)$$

Equations (22), (25) and (27) describe the membrane. These equations are used to correct the mass rate and volume rate of the plenum without the membrane.

$$\dot{M}_s = \dot{M} + \dot{M}_m \quad (29)$$

$$\dot{V}_s = \dot{V} + \dot{V}_m \quad (30)$$

where

s = denotes the system of plenum plus membrane

\dot{M} = mass flow rate of plenum

\dot{V} = volume rate of change of plenum

Using (29) and (30) in equation (6) the corrected plenum pressure rate is

$$\dot{P}_s = P_b \gamma \left(\frac{\dot{M}_s}{M} - \frac{\dot{V}_s}{V} \right)$$

where P_b , M and V are values obtained from the previous time-step calculation.

5. Model Five

Model Five is the application of equation (10) to PROGRAM TWO. It is based on the premise that the volume of the membrane could be introduced into the plenum pressure rate equation, and represent the membrane effect.

$$V_m = K P_m \tag{31}$$

$$V = V_b + V_m \tag{32}$$

Equation (31) and (32) are computed as in Model One. Then equation (32) is used in the pressure rate equation.

$$\dot{P} = P_b \gamma \left(\frac{\dot{M}}{M} - \frac{\dot{V}}{V} \right) \tag{33}$$

V. DISCUSSION OF RESULTS

A. PRESSURE RATE AND VOLUME RATE CHANGE

The addition of the pressure rate and volume rate equations was implemented without any major difficulty. In order to provide a basis of comparison for computer time analysis a quality factor "Q" was established. "Q" is defined to be the ratio of CPU execution time to problem time. For example, if the problem specified 1 minute of simulation and the CPU execution time (GO STEP in IBM COMPUTER SYSTEMS) was 5 minutes $Q = 5.0$. PROGRAMS ONE, TWO and THREE were tested with identical input parameters. The results are summarized in Table III and Table IV.

Runs were compared using PROGRAM ONE as a reference. No differences in computed output were noted for Condition One thru Four and only small changes in computed values noted with Condition Five. The integrator error tolerance levels were maintained constant for all runs.

As can be seen from the tabulated values, the addition of pressure rate and volume rate equations reduces the CPU execution time considerably for small disturbances. However, as the sea state is increased the CPU time increases. Apparently other factors in the program begin to dominate the total execution time.

TABLE III

TIMING QUALITY FACTORS20 Knots

	Program One	Program Two	Program Three
Condition One	11.25	4.8	4.50
Condition Two	13.85	6.0	5.50
Condition Three	23.0	20.5	19.2
Condition Four	42.8	28.01	22.0
Condition Five	71.0	58.1	54.0

TABLE IV

TIMING QUALITY FACTORS30 Knots

	Program One	Program Two	Program Three
Condition One	10.8	7.5	4.5
Condition Two	18.0	14.25	8.7
Condition Three	24.0	22.0	21.0
Condition Four	45.0	30.0	28.0
Condition Five	75.0	59.2	53.0

This supports the results of Reference (7) that for sea conditions the bulk of computation time is apparently in the SUBROUTINE WAVES.

It was observed that at irregular sea state two and regular sea state three water came in contact with the top of the plenum. The L&M program does not include the effect of this phenomenon in the program simulation; therefore, testing was not conducted at higher sea state conditions. The fact that water hits the top of the plenum is a reasonable condition under certain circumstances. For example, if the pitch angle is 3 degrees up the stern sinks over 6 inches. If the draft of the craft at that time is 11 inches and if the preceding wave passing the stern station is 5 inches, water should hit the top of the plenum at the stern station. The effect of this condition on total craft behavior in terms of forces and moments is not known. The effect of water contact would depend upon such factors as the length of time the wave is in contact with the top of the plenum and the area of the plenum in contact with the wave.

B. INCREASING WAVE COMPONENTS

Tests were made for irregular seas one and two using 8, 10, 15, and 20 wave components. No apparent change in output could be determined. The time at which changes in output occurred changed, but no significant reduction in output values were noted; that is the time when wave components were in-phase or out-of-phase was different, but the craft response

was the same. It was felt that if more components were used, the energy (in this case, the magnitude and frequency of the disturbing force) would be distributed over many components and that the irregular combination of these components would spread the energy of the disturbance over a larger time base. This spreading of the energy would then reduce the magnitude of the disturbance and that in turn would provide less rapid rates of change. With less rapid changes in the disturbances, the integration would take less time. The over-all time increase due to more wave components would be offset by the reduction in integration time. This is not the case; using more wave components increased CPU time. Whether 10 or less wave components are sufficient to accurately represent irregular seas was not tested.

C. MEMBRANE MODELS

A large amount of time was expended in attempting to provide adequate modeling of the plenum membrane. Model One using $V_m = K P_b$ in PROGRAM ONE did not work at all. The program would begin to execute and then stop when the integration step size was less than 1×10^{-6} .

As an aid to find the reason for this failure a computational flow diagram was drawn (See Figure 1). The addition of the correction term V_m creates an algebraic inner loop as shown by the dashed line in Fig. 1. Using a small perturbation of D in calm water and using the print switches in RHS as well as using the DEBUG option available with the G compiler, it

was observed that with Model One the values of pressure were divergent. It is not known why pressure values diverge; however, it was noted that at certain times the values of pressure and volume were increasing or decreasing together, that is when pressure was increasing while volume was increasing.

The computational flow diagram for Model Two (Figure 2) shows the inner connections of the pressure, volume and mass variables. Model Two exhibited the same symptoms and the same results as Model One, except in some cases pressure rate and volume rate rose or fell together at the same time step.

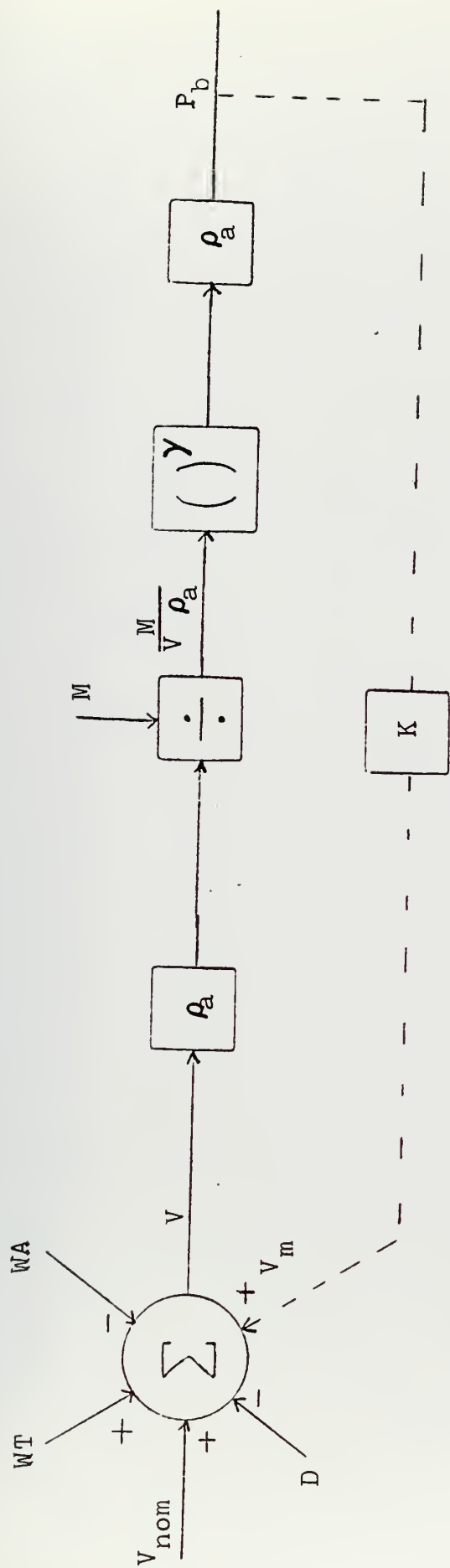
The failures of Model One and Two led to Model Three. It was felt that by correcting both pressure rate and volume rate the divergence exhibited in Models One and Two could be corrected. Model Three also failed; however, it provided the motivation to consider mass rate into the membrane. The computations performed in Model Three is shown in Figure 3.

Model Four was marginally successful. The program executes and slightly reduces the center of gravity acceleration. the reduction of the center of gravity acceleration was chosen as the criterion of whether the model was representing the membrane. This model was tested in sea state one and sea state two and provides slight reduction in the maximum values in the center of gravity acceleration. It did not reduce all of the center of gravity values. The computational flow diagram

of Model Four is given in Figure 4 and shows no algebraic loops in the RHS computations of pressure and volume rates.

Model Five was the most successful model. The computational flow is shown in Figure 5. Model Five reduced the center of gravity acceleration and for small disturbances, the pitch angle and pitch rate. For sea state one a significant reduction was observed. (See Figures 6 and 7). However, for sea state two the center of gravity accelerations were greater for the membrane when compared to the no membrane case. (See Figures 8 and 9). No reason for this could be found. The only differences in these two runs was the sea state.

One possible reason for the sea state two results, though not yet proven, could be a resonance effect at the sea state encounter frequency. Concurrent work in this area [Ref. 14] investigates the conditions for the existence of any resonance phenomena. Preliminary investigations indicate that at a wave encounter frequency of approximately 4 rad / second resonance in pitch angle occurs. The encounter frequency for regular sea state two is 5 rad / second. Whether resonance phenomena could cause this effect, however, was not determined.



(All values shown for the K^{th} iteration in RHS)

Figure 1. Computational Flow Diagram Model I

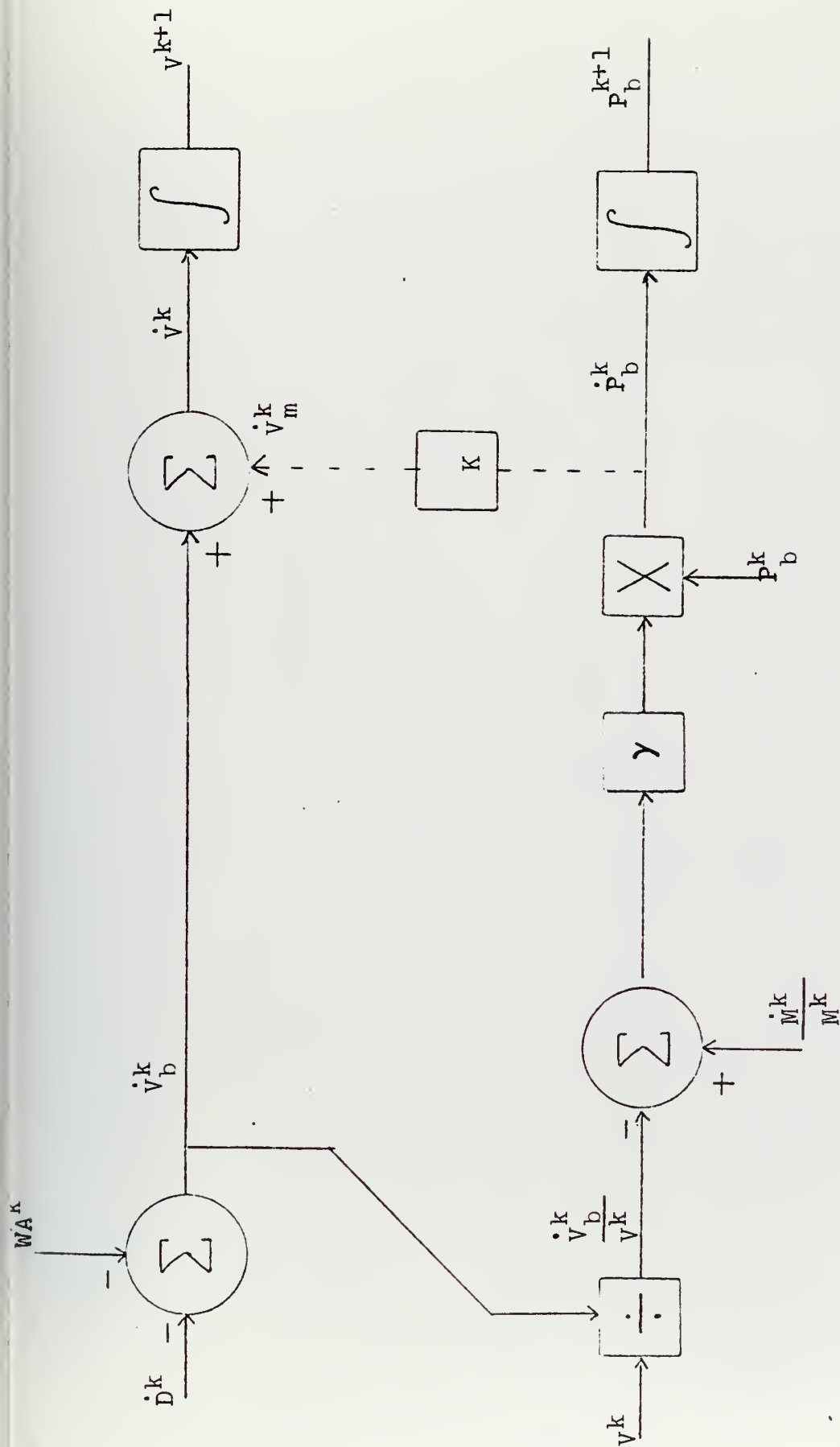


Figure 2. Computational Flow Diagram Model II

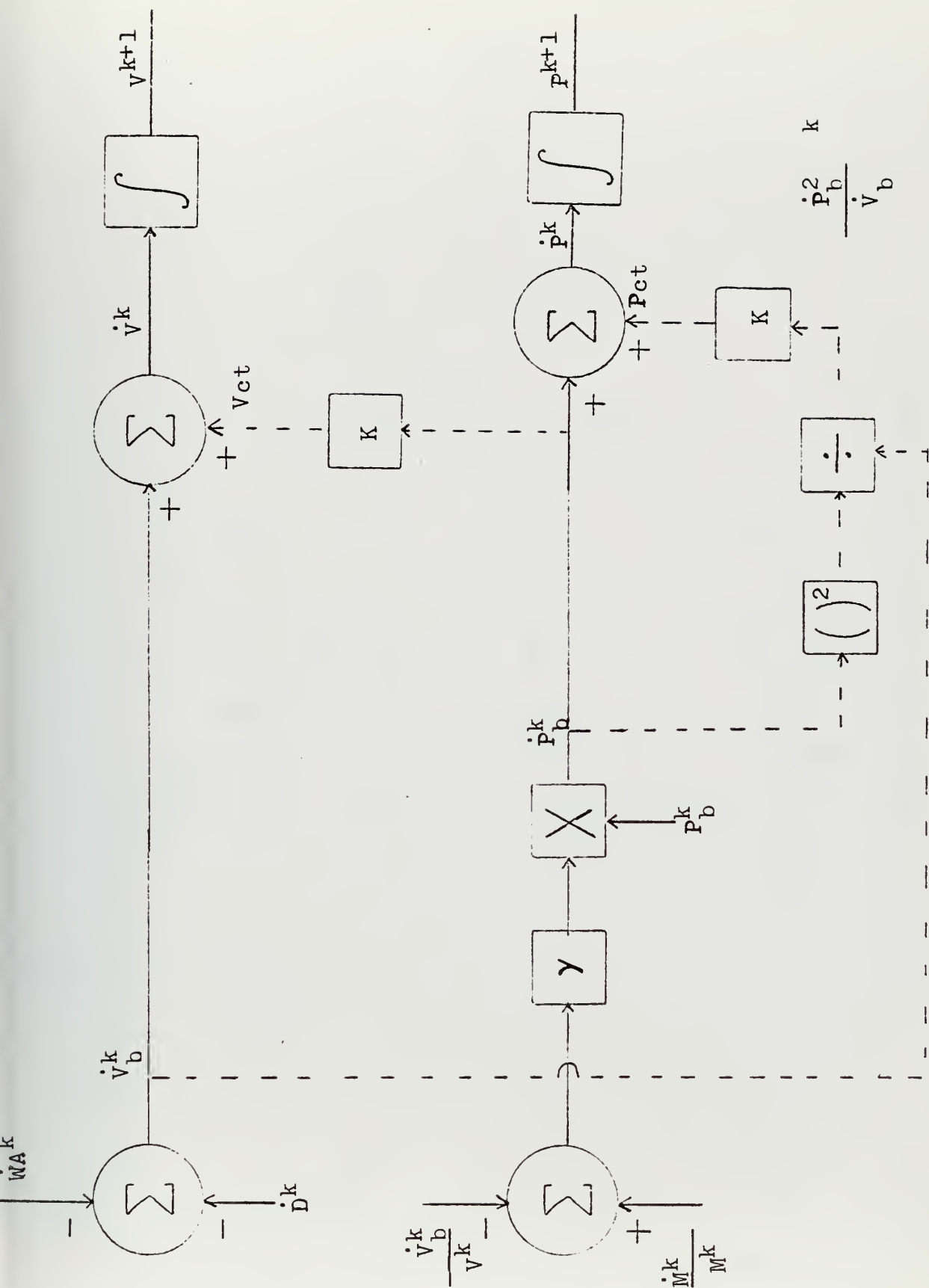


Figure 3. Computational Flow Diagram Model III

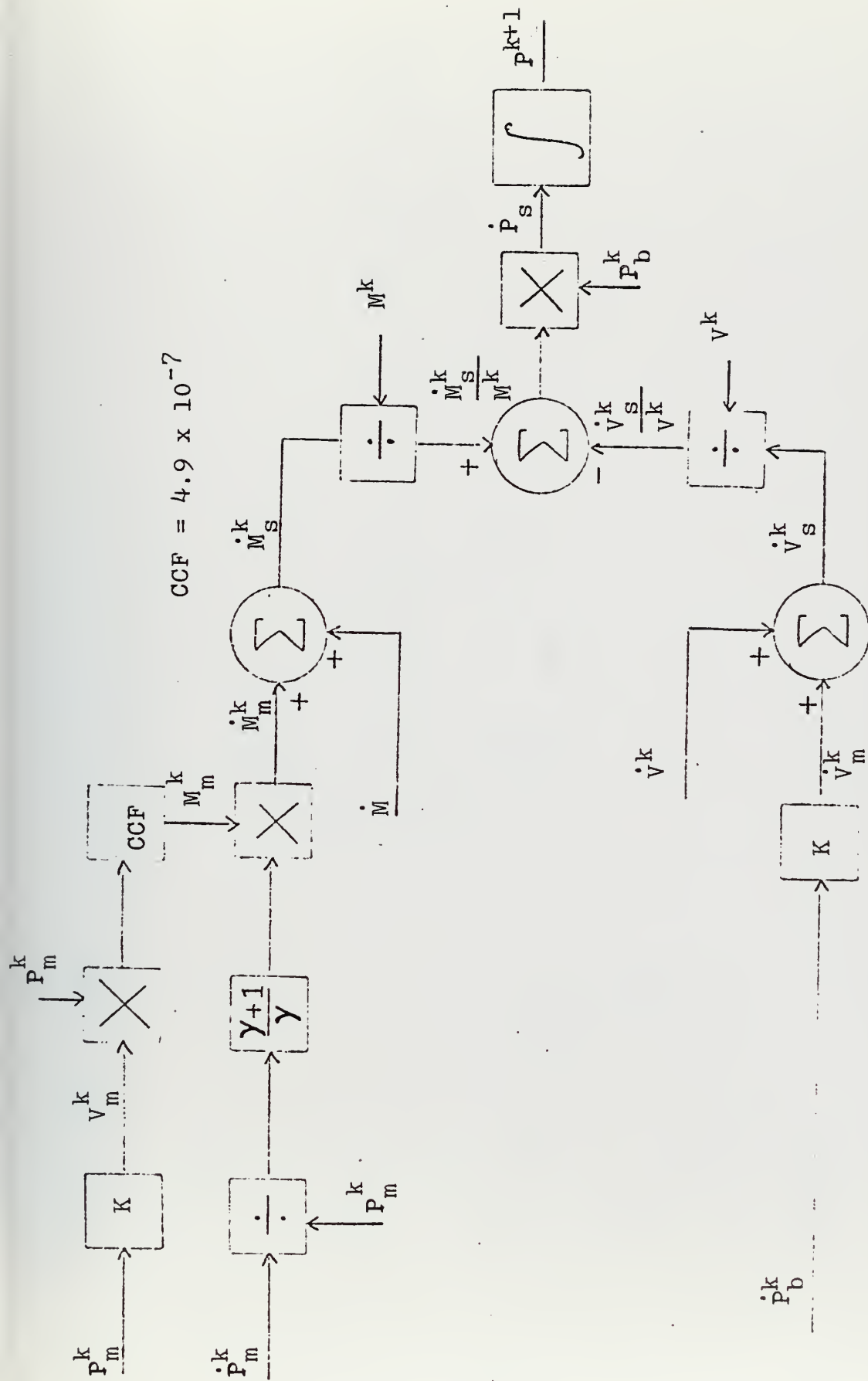


Figure 4. Computational Flow Diagram Model IV

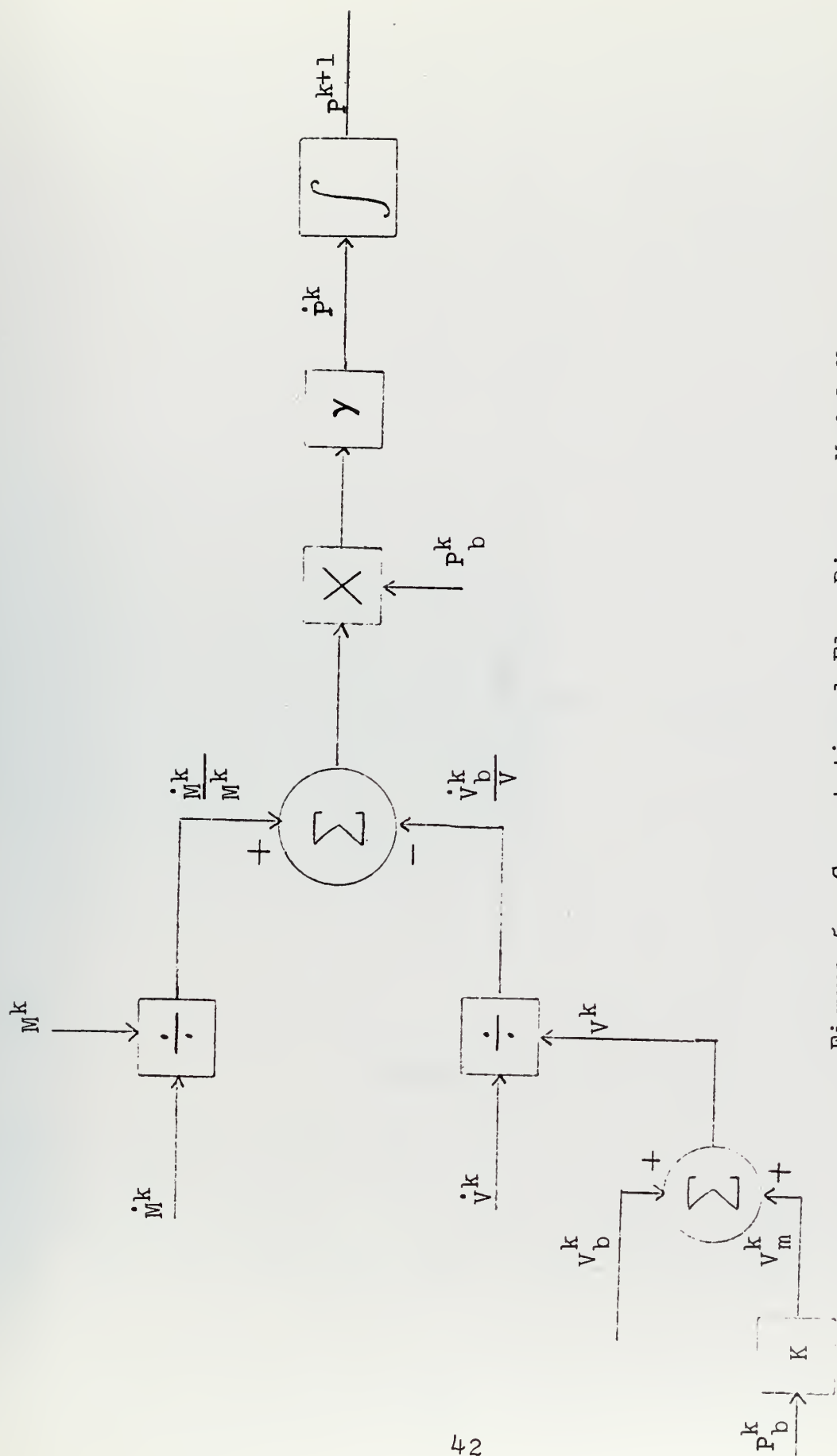


Figure 5. Computational Flow Diagram Model V

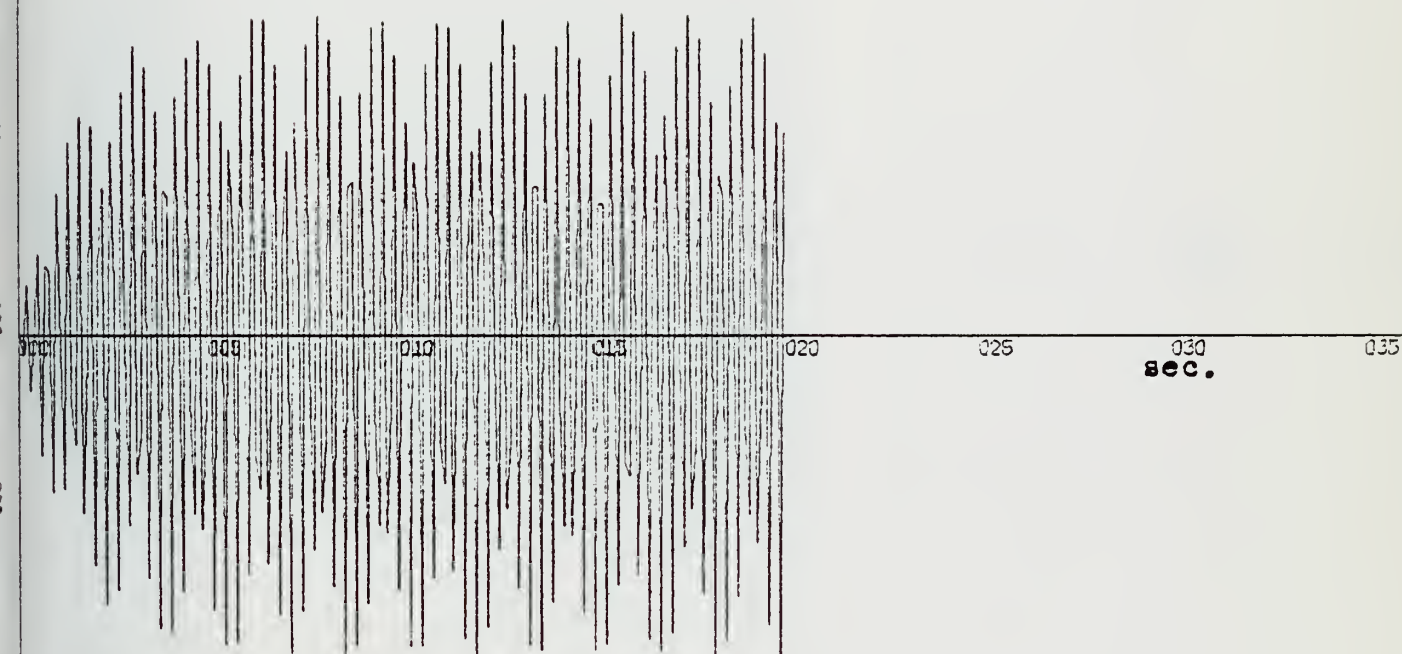


FIGURE 6

X-SCALE=5.00E+00 UNITS INCH.

Y-SCALE=5.00E-02 UNITS INCH.

PROGRAM 2 MODEL 5 20KTS REG. SEA 1

PLOT IS C.G.ACCELERATION VERSUS TIME

020
015
010
005
000
-005
-010
-015

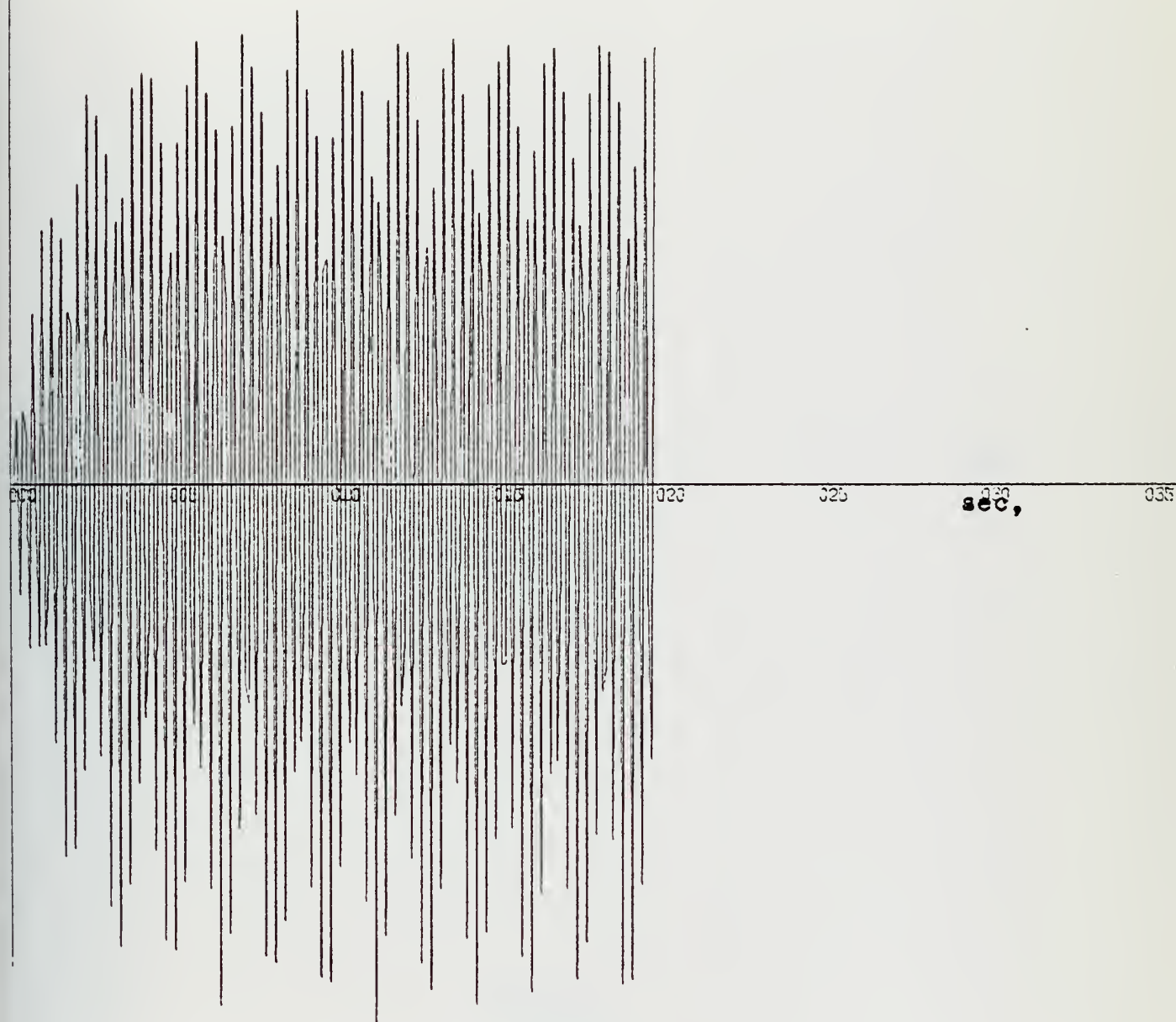


FIGURE 7

X-SCALE=5.00E+00 UNITS INCH.

Y-SCALE=5.00E-02 UNITS INCH.

PROGRAM 2 WITHOUT MEMBRANE REG. SEA 1
PLOT IS C.G. ACCELERATION VERSUS TIME

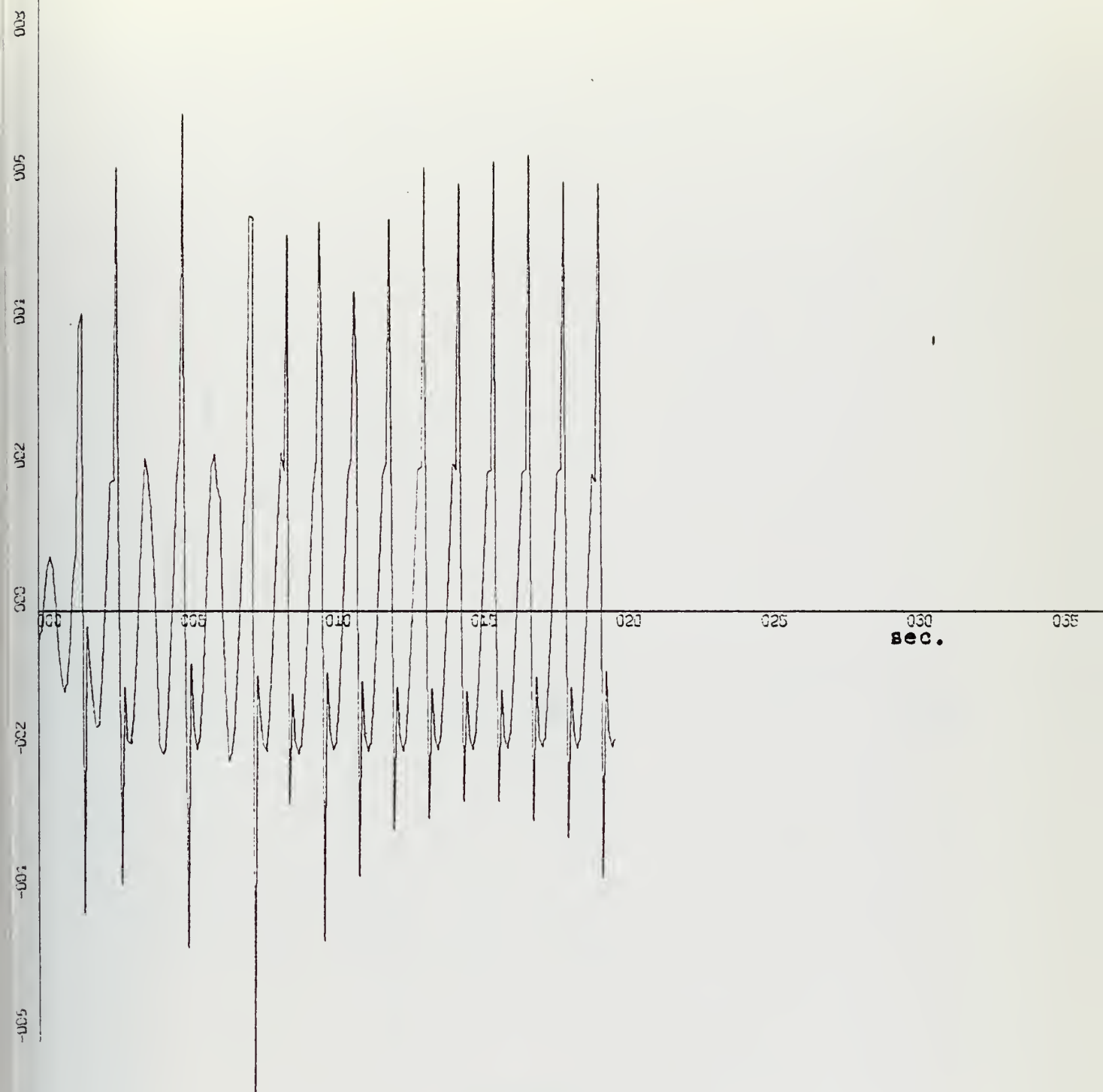


FIGURE 8

X-SCALE=5.00E+00 UNITS INCH.

Y-SCALE=2.00E-01 UNITS INCH.

PROGRAM 2 MODEL 5 20KTS REG. SEA 2

PLOT IS C.G.ACCELERATION VERSUS TIME

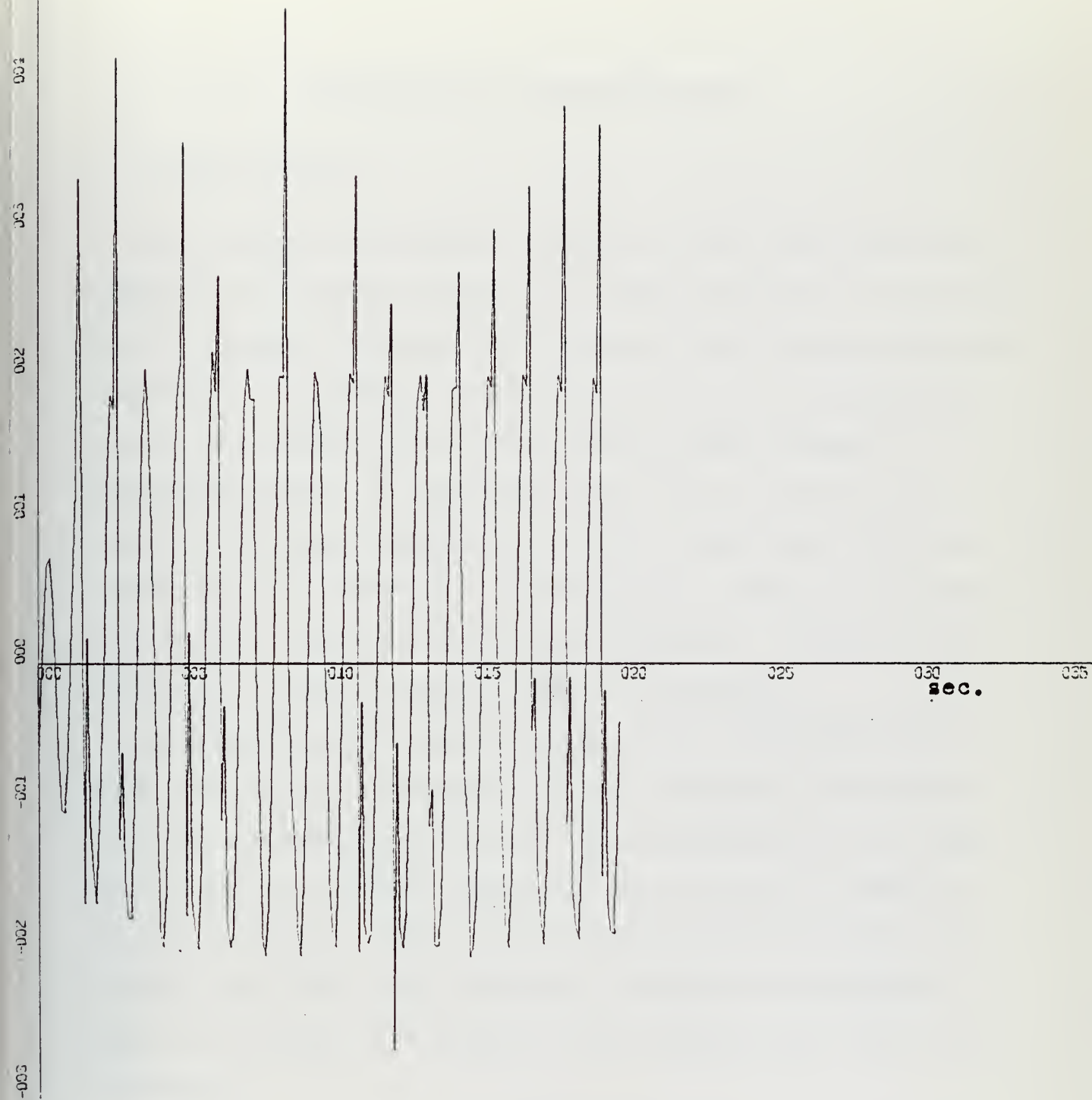


FIGURE 9

X-SCALE=5.00E+00 UNITS INCH.

Y-SCALE=1.00E-01 UNITS INCH.

PROGRAM 2 WITHOUT MEMBRANE REG. SEA 2
 PLOT IS C.G. ACCELERATION VERSUS TIME

VI. CONCLUSIONS AND RECOMMENDATIONS

A. PROGRAM TIMING

The inclusion of pressure rate and volume rate equations improved the execution time of the L&M program without decreasing the program accuracy. The changes to the program were not difficult to implement. Further effort to improve execution time of the program should be directed toward changes to SUBROUTINE WAVES. In connection with this, a study of the number of required sidewall and bow and stern seal stations should also be conducted. By reducing the number of sidewall stations the execution time should decrease. A study of the losses in accuracy, however, would be necessary.

Another facet for investigation within SUBROUTINE WAVES would be a study to determine if the trigonometric functions could be represented by the in-line programming of the expansion of sine and cosine functions, vice the use of computer library functions. Since some sine and cosine functions are nested in DO LOOPS small savings in time would accumulate. Again, the losses in accuracy to this change would have to be determined.

The elimination of SUBROUTINE DMINV did not produce any noticeable time savings but did save approximately 2 K bytes of core.

The expansion of the number of wave components did not demonstrate any time savings; however the optimum number of wave components required to simulate irregular sea conditions should be determined. A possible course of action would be to generate wave components, calculate the magnitude and frequency and compute the energy spectral density. This energy density spectrum could then be compared to the Pierson and Neumann or Moskowitz model [Ref. 11]. By determining the optimum number of wave components, a savings in CPU execution time could result.

B. ADDITIONAL MODELING

The fact that waves can hit the top of the plenum was discussed in Section V. Whether this effect produces significant forces and moments is unknown. Since the time that the wave is in contact with the plenum and the location (station numbers) is known and since the area of the plenum in contact with the waves could be approximated, (no greater than the difference between wetted stations) additional correction terms could be developed to determine whether significant forces and moments are generated by wave contact. The drag of the wetted plenum top could also be considered.

C. MEMBRANE MODELING

Of the five membrane models developed in this study, Model Five is the most usable. The accuracy of this model must be determined and the model must be validated. Whether

mass and mass flow rate terms could improve this model also needs to be determined. In this regard a detailed study of adiabatic-reversible unsteady flow conditions would be useful. This would mean the establishment of a suitable control volume and the solution of energy-work equations.

The membrane modeling in this study was for a continuous non-permeable membrane. Additional modeling for the case of a hole cut into the membrane should be attempted. The equation for a sharp-edge orifice could be used to determine air loss. The area (size) of the hole can be determined by considering as a first approximation the ratio of surface area of a hemisphere to volume of the hemisphere. As an alternative, the experimental results of the towing tank tests conducted at NSRDC, on the XR-1, using suitable scale factors, could be used to determine empirical correction factors to be applied to the Loads and Motion program.

The occurrences of algebraic loops and summation of feed forward terms as shown in the computational flow diagrams and the failure of the models in which they occur indicate that further modeling of the membrane is required. To prevent model failures, elimination of the effects of the computational loops appears to be necessary.

APPENDIX A

MEMBRANE SCALE FACTOR

The empirical relationship between pressure and volume for the membrane given in Ref. 9 is for the XR-1 test craft.

$$V_m = K P_m \quad (A1)$$

where

$$K = \frac{40 \text{ in}^3}{\text{Psf}}$$

It was therefore necessary to scale the constant K for the XR-3 test craft.

In the following development the subscript 1 refers to the XR-1 and subscript 3 refers to XR-3.

Since XR-1 and XR-3 are similar it was assumed that all dimensions scale by the ratio of plenum lengths

$$\frac{L_3}{L_1} = \lambda \quad (A2)$$

where

$$L_3 = 20 \text{ ft.}$$

$$L_1 = 5.4 \text{ ft.}$$

It was assumed that the ratio of mass to volume was constant

$$\frac{M_1}{V_1} = \frac{M_3}{V_3} = \rho \quad (A3)$$

The ratio of craft volume is

$$\frac{V_3}{V_1} = \lambda^3 \quad (\text{A4})$$

The ratio of craft pressure is

$$\frac{P_3}{P_1} = \frac{M_{3g}/A_3}{M_{1g}/A_1} \quad (\text{A5})$$

where g is the gravitational constant.

Substituting (A2) and (A3) into (A5)

$$\frac{P_3}{P_1} = \frac{V_3 A_1}{V_1 A_3} = \frac{\lambda^3}{\lambda^2} = \lambda \quad (\text{A6})$$

Using (A4) and (A6) in (A1)

$$K_1 = \frac{V_1}{P_1} \frac{V_3/\lambda^3}{P_3/\lambda} = \frac{K_3}{\lambda^2} \quad (\text{A7})$$

$$K_3 = \lambda^2 K_1 \quad (\text{A8})$$

Converting in.³ to ft.³ and using (A2)

$$K_3 = \left(\frac{20}{5.4} \right)^2 \frac{40}{1728} = .3175 \text{ ft.}^3/\text{psf} \quad (\text{A9})$$

APPENDIX B

LISTING OF FORTRAN XR-3

L&M COMPUTER PROGRAM

PROGRAM TWO MODEL FIVE

```

10 10
20 20
30 30
40 40
50 50
60 60
70 70
80 80
90 90
100 100
110 110
120 120
130 130
140 140
150 150
160 160
170 170
180 180
190 190
200 200
210 210
220 220
230 230
240 240
250 250
260 260
270 270
280 280
290 290
300 300
310 310
320 320
330 330
340 340
350 350
360 360
370 370
380 380
390 390
400 400
410 410
420 420
430 430
440 440
450 450
460 460
470 470

INTEGER ON
COMMON /AIR/ PINF,RHOINF,GAM
COMMON /BMCQ/ IMM,IMNX,IMNY,IRMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
COMMON /CONST/ PI,RAD,UO
COMMON /ENGINE/ NPS,NPP,THSTS(25),THSTP(25),XP,YP,ZP,STHS,STHP,TIP
1(25),TIS(25)
COMMON /EQNCQ/ NEQS,TOL(20),JQQ
COMMON /FPROPE/ FXP,FYP,FZP,FKP,FMP,FNP
COMMON /FROUDE/ FN,FNCRIT
COMMON /PRIME/ STIME,DELTA,DELTPNT,TPRINT
COMMON /PROMOD/ PROMO1,PROMO2,PROMO3,PROMO4,PROMO5,PROMO6,PROMO7
COMMON /PRINT/ ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,I
1RUD,IPROP,JAEROD,IRHS
COMMON /ROLL/ PHIMAX,TROLL
COMMON /RUDDR/ NPR,DELPUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,R
1CLB,RTC,RUCANG,TIR(25)
COMMON /VALOLD/ YOLD(20)
COMMON /VARBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(20),OMEGA(20),DVOLW,NWAVE,BETA,FXWAV,FY
1WAV,FZWAV,FKWAV,FMWAV,FNWAV,ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET,PB
2BAR
EQUIVALENCE (VAL(2),U), (VAL(3),V), (VAL(4),W), (VAL(5),P), (VAL(6),
1),Q), (VAL(7),R), (VAL(8),PHI), (VAL(9),THETA), (VAL(10),Z), (VAL(
211),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI), (VAL(24),PB),
3 (VAL(12),VOL)
DIMENSION DUMMY(20)
TC = 1.0
ON = 1
PI = 4.*ATAN(1.)
RAD = 180./PI
WRITE (6,12)
1 READ (4,13,END=2) DUMMY
WRITE (6,14) DUMMY
WRITE (5,13) DUMMY
GO TO 1
2 REWIND 5
3 CALL INCON (TIME)
IF (IMM.EQ.3) GO TO 11
VAL(13) = VAL(24)
C
DO 4 J=1,20
4 YOLD(J) = VAL(J+1)
C
GO TO 8
5 CONTINUE
TOLD = TIME
PBBAR = PBBAR*(1.-DELT/TC)+DELT*(PB-PINF)/TC

```



```

IF (NWAVE.LE.0) GO TO 6
ZBAR = (1.-DELT/TC)*ZBAR+DELT*Z/TC
PHIBAR = (1.-DELT/TC)*PHIBAR+DELT*PHI/TC
THEPAR = (1.-DELT/TC)*THEPAR+DELT*THETA/TC
CALL WAVES (TIME)
6 CALL SIDEWL
CALL PROP
CALL RUDDER
CALL AEROD
CALL INTGRL (TIME)
IF (TIME.GT.FTIME) GO TO 10
IF (FN.GT.FNCRIT) GO TO 7
PRINT 17
GO TO 10
7 DELOLD = TIME-TOLD
PSI = PSI+DELOLD*R
X = X+DELOLD*(U* $\cos(\text{PSI})$ -V* $\sin(\text{PSI})$ )
Y = Y+DELOLD*(U* $\sin(\text{PSI})$ +V* $\cos(\text{PSI})$ )
IF (ABS(TIME-TPRINT).LT.1.E-6) GO TO 8
GO TO 5
8 CONTINUE
IF (ITRAJ.EQ.0) GO TO 9
DPHI = PHI* $\pi$ 
DPSI = PSI* $\pi$ 
DTHETA = THETA* $\pi$ 
DP = P* $\pi$ 
DQ = Q* $\pi$ 
DR = R* $\pi$ 
VEL = 0.5925*U
WRITE (6,15) TIME,VEL,V,W,DP,DQ,DR,Z,DPHI,DTHETA,X,Y,DPSI
BETS = (-V/U)* $\pi$ 
DELRS = RUDANG* $\pi$ 
WRITE (6,16) BETS,DELRS,FXP
9 CONTINUE
IMMTAG = (IMM+1)/2
IF (IMMTAG.EQ.1.AND.TIME.GE.BTIME-1.E-8) IMT=1
TPRINT = TPRINT+DELPNT
CN = 1
GO TO 5
10 CALL COLFIL
IF (IMM.LT.1) GO TO 3
IF (IMM.NE.1) GO TO 11
END FILE IBMFIL
GO TO 3
11 CALL SAM
GO TO 3
12 FORMAT (1H1//35X,22H LISTING OF INPUT DECK//)

```

C


```

13 FORMAT (20A4)
14 FORMAT (5X,20A4)
15 FORMAT (/10X,13HTIME (SEC) = F6.2//10X,33HTRANSLATIONAL VELS (KTSMAIN 960
1) / (FT/SEC) / 10X,2HU=F6.2,5X,2HV=F6.3//10X,31HROTATIONAL VELS (KTSMAIN 970
2) VELOCITIES (DEG/SEC) / 10X,2HP=F6.2,5X,2HO=F6.2//10X,30HMAIN 980
3HDISPLACEMENTS (FT AND DEGREES) / 10X,2HZ=F7.3,5X,4HPI=F6.2,3X,6HMAIN 990
4ETA=F6.2//10X,27HTRAJECTORY (FT AND DEGREES) / 10X,2HX=F8.2,4X,2HY=FMAIN 1010
58.2,4X,4HPSI=F8.2)
16 FORMAT (1H0,9X,23HSIDESLIP ANGLE (DEG) = F8.2,10X,21HRUDDER ANGLE MAIN 1030
1 (DEG) = F8.3,10X,15HTHRUST (LBS) = F12.1)
17 FORMAT (/25X,28HCRAFT SPEED BELOW HUMP SPEED) MAIN 1040
END MAIN 1050
MAIN 1060
MAIN 1070

```

C

```

SUBROUTINE AEROD
INTEGER ON
COMMON /FAERO/ FX,FY,FZ,FK,FM,FN
COMMON /FAIR/ RHOA,XLAERO
COMMON /PROMOD/ PROMOD1,PROMOD2,PROMOD3,PROMOD4,PROMOD5,PROMOD6,PROMOD7
COMMON /PRINT/ ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,IAER 10
AER 20
AER 30
AER 40
AER 50
AER 60
AER 70
AER 80
AER 90
COMMON /VARBLE/ VAL(40)
EQUIVALENCE (VAL(2),U), (VAL(3),V), (VAL(4),W), (VAL(5),P), (VAL(6)AER 100
1),Q), (VAL(7),R), (VAL(8),PHI), (VAL(9),THETA), (VAL(10),Z), (VAL(11)AER 110
21),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI), (VAL(24),PB)AER 120
AER 130
AER 140
AER 150
AER 160
AER 170
AER 180
AER 190
AER 200
AER 210
AER 220
AER 230
AER 240
AER 250
AER 260
AER 270
AER 280
AER 290
AER 300
AER 310

```

C

```

GA = RHOA*U*U
QAL = QA*XLAERO
BETA = -V/U
BETASQ = BETA*BETA
FX = -(0.90*BETASQ+0.13)*QA
FY = (0.0*BETASQ+0.53*BETA)*QA
FZ = -(2.06*BETASQ+0.39)*QA
FK = -(0.5*BETASQ+0.0*BETA)*QAL
FM = (0.29*BETASQ+0.12)*QAL
FN = (0.0*BETASQ+0.076*BETA)*QAL
IF (IAEROD.NE.ON) RETURN
WRITE (6,1) FX,FY,FZ,FK,FM,FN

```

C

```

RETURN
1 FORMAT (/10X,23HAEROD FX,FY,FZ,FK,FM,FN/6E15.4)
END
BLOCK DATA
COMMON /AIR/ Z1(3)
COMMON /BMCO/ Z2(25)
BLDA 10
BLDA 20
BLDA 30

```

COMMON / COLUMN/ Z3(2)
COMMON / CONST/ Z4(3)
COMMON / CNTRL/ Z5(10)
COMMON / ENGINE/ Z6(107)
COMMON / EQNCO/ Z7(22)
COMMON / FAERO/ Z8(6)
COMMON / FAIR/ Z9(2)
COMMON / FANMAP/ Z10(262)
COMMON / FORBS/ Z11(7)
COMMON / FORSS/ Z12(8)
COMMON / FPROP/ Z13(6)
COMMON / FROUDE/ Z14(2)
COMMON / FRUD/ Z15(6)
COMMON / GBCW/ Z16(1)
COMMON / GEOM/ Z17(138)
COMMON / GEOMBS/ Z18(62)
COMMON / GEOMSS/ Z19(62)
COMMON / GEOMSW/ Z20(11)
COMMON / KSWTCH/ Z21(1)
COMMON / LEAKER/ Z22(4)
COMMON / MASSES/ Z23(817)
COMMON / MATRIX/ Z24(36)
COMMON / MSIDW/ Z25(55)
COMMON / MWAVE/ Z26(12)
COMMON / OPTION/ Z27(4)
COMMON / PLENUM/ Z28(7)
COMMON / PRIME/ Z29(5)
COMMON / PRINT/ Z30(12)
COMMON / PWAVE/ Z31(2)
COMMON / RISER/ Z32(1)
COMMON / ROLL/ Z33(2)
COMMON / RUDDR/ Z34(62)
COMMON / SIDE/ Z35(22)
COMMON / SOFTBS/ Z36(20)
COMMON / SOFTSS/ Z37(19)
COMMON / STABLE/ Z38(5)
COMMON / STSLR/ Z39(2)
COMMON / VALOLD/ Z40(20)
COMMON / VARBLE/ Z41(40)
COMMON / WAVE/ Z42(100)
COMMON / WAVEF/ Z43(80)
COMMON / SLOPE/ Z44(5)
COMMON / PROMOD/ Z45(7)
DATA Z1/3*0.0/
DATA Z2/25*0.0/
DATA Z3/2*0.0/
DATA Z4/3*0.0/
DATA Z5/10*0.0/

BLDA 40
BLDA 50
BLDA 60
BLDA 70
BLDA 80
BLDA 90
BLDA 100
BLDA 110
BLDA 120
BLDA 130
BLDA 140
BLDA 150
BLDA 160
BLDA 170
BLDA 180
BLDA 190
BLDA 200
BLDA 210
BLDA 220
BLDA 230
BLDA 240
BLDA 250
BLDA 260
BLDA 270
BLDA 280
BLDA 290
BLDA 300
BLDA 310
BLDA 320
BLDA 330
BLDA 340
BLDA 350
BLDA 360
BLDA 370
BLDA 380
BLDA 390
BLDA 400
BLDA 410
BLDA 420
BLDA 430
BLDA 440
BLDA 450
BLDA 460
BLDA 470
BLDA 480
BLDA 490
BLDA 500
BLDA 510

```

DATA Z6/107*0.0/
DATA Z7/21*0.0/
DATA Z8/6*0.0/
DATA Z9/2*0.0/
DATA Z10/262*0.0/
DATA Z11/7*0.0/
DATA Z12/8*0.0/
DATA Z13/6*0.0/
DATA Z14/2*0.0/
DATA Z15/6*0.0/
DATA Z16/0.0/
DATA Z17/138*0.0/
DATA Z18/62*0.0/
DATA Z19/62*0.0/
DATA Z20/11*0.0/
DATA Z21/0.0/
DATA Z22/4*0.0/
DATA Z23/817*0.0/
DATA Z24/36*0.0/
DATA Z25/55*0.0/
DATA Z26/12*0.0/
DATA Z27/4*0.0/
DATA Z28/7*0.0/
DATA Z29/5*0.0/
DATA Z30/12*0.0/
DATA Z31/2*0.0/
DATA Z32/0.0/
DATA Z33/2*0.0/
DATA Z34/62*0.0/
DATA Z35/22*0.0/
DATA Z36/20*0.0/
DATA Z37/19*0.0/
DATA Z38/5*0.0/
DATA Z39/2*0.0/
DATA Z40/20*0.0/
DATA Z41/40*0.0/
DATA Z42/100*0.0/
DATA Z43/80*0.0/
DATA Z44/5*0.0/
DATA Z45/7*0.0/
END

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SUBROUTINE BOWSL

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INTEGER CN
COMMON /AIR/ PINF,RHGINF,GAM
COMMON /CONST/ PI,RAD,UO
COMMON /FORBS/ FX,FY,FZ,FK,FM,FN,QL

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BLDA 520
BLDA 530
BLDA 540
BLDA 550
BLDA 560
BLDA 570
BLDA 580
BLDA 590
BLDA 600
BLDA 610
BLDA 620
BLDA 630
BLDA 640
BLDA 650
BLDA 660
BLDA 670
BLDA 680
BLDA 690
BLDA 700
BLDA 710
BLDA 720
BLDA 730
BLDA 740
BLDA 750
BLDA 760
BLDA 770
BLDA 780
BLDA 790
BLDA 800
BLDA 810
BLDA 820
BLDA 830
BLDA 840
BLDA 850
BLDA 860
BLDA 870
BLDA 880
BLDA 890
BLDA 900
BLDA 910
BLDA 920

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BWSL 10
BWSL 20
BWSL 30
BWSL 40
BWSL 50
BWSL 60

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COMMON /GEOM/ WIDTH,XL,XX(4,11),YY(4,11),NSTA(4),AB,VOLNOM,DELS(4,BWSL
110),XCP,ZCP BWSL 80
COMMON /GEOMBS/ DETABX(11),DETABT(11),ARM1B(10),ARM2B(10),DFBS(10) BWSL 80
1,TSKIB(10) BWSL 100
COMMON /LEAKER/ ALEAK,BLEAK,CFSS,CFBS BWSL 110
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,AMBWSL 120
1I(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO BWSL 130
COMMON /PRINT/ ON,IACCEL,IVEL,ITRAJ,ISIDLW,IBOWSL,ISTNSL,IWAVES,IBWSL 140
1RUD,IPROP,IAEROD,IRHS BWSL 150
COMMON /PROMOD/ PROMO1,PROMO2,PROMO3,PROMO4,PROMO5,PROMO6,PROMO7 BWSL 160
COMMON /SLOPE/ WATSLP,XLPWV,XLXPWV,PWVHT,XPWVXS BWSL 170
COMMON /SOFTBS/ XBF,PBS,SINBS,COSBS,XBS,ZBS,DELYBS,DPBS,FLMAXB,YAV BWSL 180
1GB(10),CENCAB BWSL 190
COMMON /VARBLE/ VAL(40) BWSL 200
COMMON /WAVE/ ETA(4,11),AW(20),OMEGA(20),DVOLW,NWAVE,BETA,FXWAV,FYBWSL 210
1WAV,FZWAV,FKWAV,FMWAV,FNWAV,ZBAR,PHIBAR,THEBAR,TC,COSRET,SINRET,PBBWSL 220
2BAR BWSL 230
DIMENSION FLKID(11), WETLEN(11), BWSL(6,24), GAP(11), ELSKI(11), BWSL 240
1DPFT(11) BWSL 250
DATA ENU,HNGHT/1.28F-5,1.875/ BWSL 260
DATA BWSL/0.0,3.8,6.9,9.9,12.3,15.0,0.0,4.1,7.3,10.5,13.2,15.7,0.0,0.8BWSL 270
24,15.4,18.3,0.0,5.5,9.6,13.3,16.1,19.6,0.0,5.8,9.9,13.8,17.1,20.6,BWSL 280
30,0.6,1.1,10.6,14.7,18.4,21.9,0.0,6.4,11.0,15.3,19.3,23.3,0.0,6.6,11BWSL 290
4.7,16.4,20.5,24.5,0.0,6.9,12.3,17.6,22.1,25.7,0.0,7.2,13.5,19.6,24BWSL 300
5.1,18.3,0.0,8.2,15.3,21.7,26.3,31.3,0.0,9.6,17.5,24.2,29.7,34.6,0BWSL 310
60,11.9,20.0,26.7,32.3,38.0,0.0,14.0,22.5,30.0,35.8,41.0,0.0,17.5,2BWSL 320
75.5,32.5,39.7,44.5,0.0,21.0,30.0,37.4,42.0,47.0,0.0,24.6,33.7,41.0BWSL 330
8,45.0,48.7,0.0,29.4,38.5,45.0,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48BWSL 340
9,7.0,0.0,40.0,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48BWSL 350
$8.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48.7,48BWSL 360
DATA CORLEN/3.75/ BWSL 370
EQUIVALENCE (VAL(1),TIME), (VAL(2),U), (VAL(3),V), (VAL(4),W), (VABWSL 380
1L(5),P), (VAL(6),Q), (VAL(7),R), (VAL(8),PHI), (VAL(9),THETA), (VABWSL 390
2L(10),Z), (VAL(11),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI) BWSL 400
3, (VAL(24),PB) BWSL 410
DO 1 J=1,11 BWSL 420
GAP(J) = 0.0 BWSL 430
ELSKI(J) = 0.0 BWSL 440
WETLEN(J) = 0.0 BWSL 450
ELSKID(J) = 0.0 BWSL 460
1 CONTINUE BWSL 470
ALBS = 0.0 BWSL 480
FX = 0.0 BWSL 490
FX = 0.0 BWSL 500
FX = 0.0 BWSL 510
FX = 0.0 BWSL 520
FX = 0.0 BWSL 530
FX = 0.0 BWSL 540

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```

FK = 0.0
FM = 0.0
FN = 0.0
DELPBG = PBS-PB
IF (DELPBG.LT.0.0) DELPBG=0.0
PBAR = PB-PINF
DELP = PBAR
IF (DELP.LT.0.0) DELP=0.0
ARGO = ELMAXB/CORLEN
ARGO = ARSIN(ARGO)
X1 = XBS+ZBS*THETA-CORLEN*COS(ANGO)
Z1 = -Z-ZBS+XBS*THETA-ELMAXB*CCS(THETA)
DPHTFT = (5.5/(1.+(U/25.))**2)*0.0833
IF (CENCAB.GT.1.1875) CENCAB=1.1875
N = NSTA(3)

DO 3 K=1,N
DPFT(K) = DPHTFT
ELSKI(K) = (ETA(3,K)-DETABX(K)*(XX(3,K)-X1)-Z1)+YY(3,K)*PHI+XLXPWV
1*WATSLP
IF (ELSKI(K).GT.HINGHT) ELSKI(K)=HINGHT
IF ((HINGHT-ELSKI(K)+DPFT(K)).GE.ELMAXB) DPFT(K)=ELMAXB-HINGHT+ELSKID(K)
1KI(K)
IF (DPFT(K).LT.0.0) DPFT(K)=0.0
ELSKID(K) = (ELSKI(K)-DPFT(K))*12.0
IF ((HINGHT-ELSKID(K)/12.0).GE.ELMAXB) ELSKID(K)=(HINGHT-ELMAXB)*12.0
DPIN = DPFT(K)*12.0
MM1 = DPIN
MM2 = MM1+1
DINC = DPIN-MM
GAP(K) = -ELSKI(K)+(HINGHT-ELMAXB)
IF (GAP(K).LT.0.0) GAP(K)=0.0
IF (ELSKID(K).GE.0.) GO TO 2
WETLEN(K) = ELSKI(K)
GO TO 3
2 MM3 = ELSKID(K)
MM4 = MM3+1
MM5 = MM4+1
DLINC = ELSKID(K)-MM3
BWSL1 = BWSL(MM1,MM4)
BWSL2 = BWSL(MM1,MM5)
BWSL3 = BWSL(MM2,MM4)
BWSL4 = BWSL(MM2,MM5)
BWSLA1 = (BWSL2-BWSL1)*DLINC+BWSL1
BWSLA2 = (BWSL4-BWSL3)*DLINC+BWSL3
WETLEN(K) = ((BWSLA2-BWSLA1)*DINC+BWSLA1)*0.08333

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BWSL 550
BWSL 560
BWSL 570
BWSL 580
BWSL 590
BWSL 600
BWSL 610
BWSL 620
BWSL 630
BWSL 640
BWSL 650
BWSL 660
BWSL 670
BWSL 680
BWSL 690
BWSL 700
BWSL 710
BWSL 720
BWSL 730
BWSL 740
BWSL 750
BWSL 760
BWSL 770
BWSL 780
BWSL 790
BWSL 800
BWSL 810
BWSL 820
BWSL 830
BWSL 840
BWSL 850
BWSL 860
BWSL 870
BWSL 880
BWSL 890
BWSL 900
BWSL 910
BWSL 920
BWSL 930
BWSL 940
BWSL 950
BWSL 960
BWSL 970
BWSL 980
BWSL 990
BWSL 1000
BWSL 1010
BWSL 1020

C

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3 CONTINUE
C
N = NSTA(3)-1
DO 10 J=1,N
WETLAV = (WETLEN(J+1)+WETLEN(J))*0.5
IF (WETLAV.LE.0.001) GO TO 8
DPFTAV = (DPFT(J+1)+DPFT(J))*0.5
ELSKIA = (ELSKI(J+1)+ELSKI(J))*0.5
ELSKDA = (ELSKID(J+1)+ELSKID(J))*0.04166
SEALHT = HINGHT-ELSKDA
DIFF = 2.0*CENCAB-(SEALHT+0.5)
IF (DIFF.GT.0.5) DIFF=0.5
ARM1B(J) = X1+WETLAV*0.5
ARM2B(J) = ZS-ELSKIA+DPFTAV*0.5
IF (DIFF.GE.0.25) GO TO 4
DFBS(J) = -DELPA*DELYBS*WETLAV
GO TO 7
4 FORLEN = XBF-WETLAV
IF (FORLEN.EQ.0.0) GO TO 5
ARGW = (HINGHT-ELSKIA)/FORLEN
IF (ARGW.GT.1.0) ARGW=1.0
ANGW = ARSIN(ARGW)
EURCOS = COS(ANGW)
GO TO 6
5 FORCOS = 0.0
6 DFBS(J) = -DELPA*DELYBS*WETLAV-DELPA*FORLEN*DELYBS*FORCOS*((FORLEN*0.5*FORCOS)/(FORLEN*FORCOS+WETLAV/2.0))*((DIFF-0.25)*4.0)
7 ARG = 0.5*RHO*U*WETLAV*DELYBS
RESKI = U*WETLAV/ENU
CDTSKI = 0.427/(ALOG10(RESKI)-0.407)**2.64
TSKIB(J) = -ARG*CDTSKI
GO TO 9
8 DFBS(J) = 0.0
TSKIB(J) = 0.0
9 CONTINUE
FX = FZ+DFBS(J)
FK = FK+DFBS(J)*YAVGB(J)
FM = FM-DFBS(J)*ARM1B(J)+TSKIB(J)*ARM2B(J)
FN = FN-TSKIB(J)*YAVGB(J)
ALBS = ALBS+(GAP(J)+GAP(J+1))*DELYBS*0.5
10 CONTINUE
C
ALBS = ALBS+BLEAK
SQFAC = SQRT(2.*ABS(PBAR)/RHOINF)
QL = CFBS*ALBS*SQFAC*SIGN(1.,PBAR)
IF (IBCSL.NE.ON) RETURN

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C      WRITE (6,11) GAP,WETLEN,FX,FY,FZ,FK,FM,FN
C
C      RETURN
C
11  FORMAT (//10X,8HBOW SEAL/26H GAP (FT.) (PORT TO STBD.)/11F10.5/28HBOWSL1510
1  WETLEN(FT.) (PORT TO STBD.)/11F10.5/10X,23HBOWSL FX,FY,FZ,FK,FM,FN,FBWBSL1520
2  N/6E15.4)BWSL1530
ENDBWSL1540
BWSL1550
11  FORMAT (//10X,8HBOW SEAL/26H GAP (FT.) (PORT TO STBD.)/11F10.5/28HBOWSL1560
1  WETLEN(FT.) (PORT TO STBD.)/11F10.5/10X,23HBOWSL FX,FY,FZ,FK,FM,FN,FBWBSL1570
2  N/6E15.4)BWSL1580
ENDBWSL1590

SUBROUTINE COLFIL
COMMON /AXIS/ NXYS(26)
COMMON /COLUMN/ IVERT, ILATRL
COMMON /CURVE/ NCURV(10)
COMMON /EQNCO/ NEQS,TOL(20),JQQ
COMMON /GRAF/ NGRAF,NDRW
COMMON /HEADG/ TICRD(6)
COMMON /PROMOD/ PROMO1,PROMO2,PROMO3,PROMO4,PROMO5,PROMO6,PROMO7
COMMON /STEP/ STEP2
COMMON /SUM/ ISUM1(8),ISUM2(8)
REAL *8TICRD
REAL LABEL
REAL LAB(4),,1.,,2.,,3./
REAL *8NAMES(52)/,TIME,,WAVEHEI,,GHT,,ZDISPLA,,CEMENT,,PITCFL
1CHAN,,GLE,,PLENUMP,,RESSURE,,BOWACCE,,LEFPACTION,,C.G.ACCE,,LCFL
2ERATION,,FANPOWE,,R(IDEAL),,ROLLANG,,LE,,YAWWANG,,E,,LATACCCFL
3E,,LERATION,,SPEFETH,,RUWATER,,TURNRAD,,IUS,,PLENUMV,,DUMECFL
4,,XDISPLA,,CEMENT,,YDISPLA,,CEMENT,,AIRFLOW,,IN,,AIRFLOW,,THCFL
5CUT,,NETFORC,,EXDIF,,WAVEFOR,,CFXDIR,,THRUSTS,,TARBOARD,,RUCFL
6RUSTP,,ORTSIDE,,PITCH,,RATE,,ROLL,,RATE,,YAW,,RUDDERFL
7A,,NGLE,,
REAL *8TITLE(12)
REAL *8LINE2(2),,PLOTIS,,VERPUS,/
REAL *8LAMEX(2),,NAMEFY(2),,NAME(16)
REAL *8NAMEX(TITLE(1),TICRD(1)),(TITLE(2),TICRD(2)),(TITLE(3),TICRD(3)),(TITLE(4),TICRD(4)),(TITLE(5),TICRD(5)),(TITLE(6),TICRD(6)),(TITLE(7),TICRD(7)),(TITLE(8),TICRD(8)),(TITLE(9),TICRD(9)),(TITLE(10),TICRD(10)),(TITLE(11),TICRD(11)),(TITLE(12),TICRD(12))
1CRD(3)),(TITLE(4),TICRD(4)),(TITLE(5),TICRD(5)),(TITLE(6),TICRD(6)),(TITLE(7),TICRD(7)),(TITLE(8),TICRD(8)),(TITLE(9),TICRD(9)),(TITLE(10),TICRD(10)),(TITLE(11),TICRD(11)),(TITLE(12),TICRD(12))
2(6))
DIMENSION PVQQ(26), XOUT(900), YOUT(900), AFIL(8)
DIMENSION THSTS(1), THSTP(1)
EQUIVALENCE (PVQQ(1),TIME), (PVQQ(2),ETA), (PVQQ(3),Z), (PVQQ(4),TICFL
1HETA), (PVQQ(5),PB), (PVQQ(6),BOWACC), (PVQQ(7),ACC), (PVQQ(8),FANCCFL
2PWR), (PVQQ(9),PHI), (PVQQ(10),BETAS), (PVQQ(11),ACCLAT), (PVQQ(12),CCFL
3),U), (PVQQ(13),TRADUS), (PVQQ(14),VOLP), (PVQQ(15),X), (PVQQ(16),FCFL
4Y), (PVQQ(17),QIN), (PVQQ(18),QOUT), (PVQQ(19),GFXX), (PVQQ(20),FCFL
5XPWAV), (PVQQ(21),THSTS(1)), (PVQQ(22),THSTP(1)), (PVQQ(23),QDEG), (PVQQ(24),PDEG), (PVQQ(25),PDEG), (PVQQ(26),DELR)
6 (PVQQ(24),PDEG), (PVQQ(25),PDEG), (PVQQ(26),DELR)

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```

IF (JQQ.NE.2) GO TO 1
WRITE (6,23) STEP2
1 END FILE 1
REWIND 1
TITLE(7) = LINE2(1)
TITLE(10) = LINE2(2)
IF (NGRAF.EQ.0) GO TO 7
J = 1
NGF = NGRAF
INDEX = NGRAF#2
C
DO 6 I=1, INDEX, 2
INDX = NXYS(I)
INDY = NXYS(I+1)
IQ = 0
2 READ (1, END = 8) TIME, ETA, Z, THETA, PB, BOWACC, ACC, FANPWR, PHI, BETAS, A
1CCLAT, U, TRADUS, VOLP, X, Y, QIN, QOUT, GFXXX, FXPWAV, THSTS(1), THSTP(1), QDC
2FG, PDEG, RDEG, DELRS
IF (IQ.GE.900) GO TO 3
IQ = IQ+1
XOUT(IQ) = PVQQ(INDX)
YOUT(IQ) = PVQQ(INDY)
GO TO 2
3 REWIND 1
INX = INDX*2
INY = INDX*2
NAMEX(1) = NAMES(INX-1)
NAMEX(2) = NAMES(INX)
NAMEY(1) = NAMES(INY-1)
NAMEY(2) = NAMES(INY)
IF (NDRW.EQ.1) GO TO 4
C
CALL PLOTP (XOUT, YOUT, -IQ, 0)
C
WRITE (6,24) NAMEX, NAMEY
GO TO 6
4 TITLE(8) = NAMEX(1)
TITLE(9) = NAMEX(2)
TITLE(11) = NAMEX(1)
TITLE(12) = NAMEX(2)
NCUR = NCURV(J)
IF (NCUR.NE.0) GO TO 5
LABEL = LAB(1)
C
CALL DRAW (IQ, XOUT, YOUT, NCUR, 0, LABEL, TITLE, 0, 0, 0, 0, 0, 0, 8, 8, 0, LAST)
C
J = J+1
GO TO 6
CFL 390
CFL 400
CFL 410
CFL 420
CFL 430
CFL 440
CFL 450
CFL 460
CFL 470
CFL 480
CFL 490
CFL 500
CFL 510
CFL 520
CFL 530
CFL 540
CFL 550
CFL 560
CFL 570
CFL 580
CFL 590
CFL 600
CFL 610
CFL 620
CFL 630
CFL 640
CFL 650
CFL 660
CFL 670
CFL 680
CFL 690
CFL 700
CFL 710
CFL 720
CFL 730
CFL 740
CFL 750
CFL 760
CFL 770
CFL 780
CFL 790
CFL 800
CFL 810
CFL 820
CFL 830
CFL 840
CFL 850
CFL 860

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C      5 WRITE (2) IQ,NCUR,NGF,LABEL,(TITLE(K),K=1,12),(XOUT(L),YOUT(L),L=1,CFL
      6 NGF = NGF-1
      7 CONTINUE
      8 IF ((NGF.EQ.0).AND.(NCUR.EQ.3)) GO TO 13
      9 IF (IVERT.NE.1) GO TO 16
     10 K = 0
     11 DO 8 I=1,8
     12 IF (ISUM1(I).NE.0) K=K+1
     13 CONTINUE
     14 NUM1 = K
     15 IF (K.EQ.0) GO TO 16
     16 N = K*2
     17 J = 1
     18 DO 9 I=1,NUM1
     19 INDEX = ISUM1(I)*2
     20 INAME(J) = NAMES(IX-1)
     21 INAME(J+1) = NAMES(IX)
     22 J = J+2
     23 CONTINUE
     24 9 CONTINUE
     25 WRITE (6,26) (INAME(I),I=1,N)
     26 GO TO 14
     27 END FILE 2
     28 REWIND 2
     29 NGF = NGRAF
     30 J = 1
     31 READ (2,END = 38) IQ,NCUR,NGRAF,LABEL,(TITLE(K),K=1,12),(XOUT(L),Y
     32 OUT(L),L=1,IQ)
     33 IF ((NGF.EQ.INGRAF).AND.(NCUR.EQ.J)) GO TO 12
     34 GO TO 11
     35 LABEL = LAB(J+1)
     36 CALL DRAW (IQ,XOUT,YOUT,NCUP,0,LABEL,TITLE,0,0,0,0,8,8,0,LAST)
     37 REWIND 2
     38 J = J+1
     39 IF (J.EQ.4) GO TO 13
     40 GO TO 11
     41 13 NGF = NGF-1
     42 IF (NGF.EQ.0) GO TO 7
     43 J = 1
     44 GO TO 11

```

```

C      14 READ (1,END = 13) (PVQQ(I),I=1,26)
      DO 15 I=1,NUM1
      J = ISUM1(I)
      15 AFILE(I) = PVQQ(J)
C
      WRITE (6,27) (AFILE(I),I=1,NUM1)
      GO TO 14
      REWIND 1
      16 IF (ILATRL.NE.1) GO TO 22
      WRITE (6,28)
      K = 0
C
      DO 17 I=1,8
      IF (ISUM2(I).NE.0) K=K+1
      17 CONTINUE
C
      NUM2 = K
      IF (K.EC.0) GO TO 21
      N = K*2
      J = 1
C
      DO 18 I=1,NUM2
      INDEX = ISUM2(I)*2
      INAME(J) = NAMES(INDEX-1)
      INAME(J+1) = NAMES(INDEX)
      J = J+2
      18 CONTINUE
C
      WRITE (6,26) (INAME(I),I=1,N)
      19 READ (1,END = 16) (PVQQ(I),I=1,26)
C
      DO 20 I=1,NUM2
      J = ISUM2(I)
      20 AFILE(I) = PVQQ(J)
C
      WRITE (6,27) (AFILE(I),I=1,NUM2)
      GO TO 19
      REWIND 1
      22 RETURN
C
      23 FORMAT ('0',4X,'THIS RUN USED VARIABLE STEP SIZE',/, '0',4X,'THE MINIMUM STEP SIZE',/, '0',4X,'THE MAXIMUM STEP SIZE',/, '0',4X,'THE RUN WAS',2X,F30.5)
      24 FORMAT (' ',20X,2A8,' IS THE INDEPENDENT VARIABLE AND ',2A8,' THE INDEPENDENT VARIABLE')
      25 FORMAT ('0',50X,'***SUMMARY ONE***',/, '0')
      26 FORMAT ('0',16A8)
      27 FORMAT ('0',8(3X,F10.2,3X))

```

CFL 1350
 CFL 1360
 CFL 1370
 CFL 1380
 CFL 1390
 CFL 1400
 CFL 1410
 CFL 1420
 CFL 1430
 CFL 1440
 CFL 1450
 CFL 1460
 CFL 1470
 CFL 1480
 CFL 1490
 CFL 1500
 CFL 1510
 CFL 1520
 CFL 1530
 CFL 1540
 CFL 1550
 CFL 1560
 CFL 1570
 CFL 1580
 CFL 1590
 CFL 1600
 CFL 1610
 CFL 1620
 CFL 1630
 CFL 1640
 CFL 1650
 CFL 1660
 CFL 1670
 CFL 1680
 CFL 1690
 CFL 1700
 CFL 1710
 CFL 1720
 CFL 1730
 CFL 1740
 CFL 1750
 CFL 1760
 CFL 1770
 CFL 1780
 CFL 1790
 CFL 1800
 CFL 1810
 CFL 1820

28 FORMAT ('0',50X,'***SUMMARY TWO***',/, '0')
END

CFL 1830
CFL 1840

SUBROUTINE FAN

```

INTEGER ON
COMMON /AIR/ PINF, RHOINF, GAM
COMMON /FANAP/ QIN, QBAN(25), QMFAN(25), QSFAN(25), ENBFAN, ENMFAN, ENFAN
1SFAN, BRPM, EMRPM, SRPM, NPTSB, NPTSS, PBFAN(25), PMFAN(25), PSFAN(25)
25), TMEB(25), DELB(25), NB, TMEB(25), DELS(25), NS
COMMON /PROMOD/ PROMO1, PROMO2, PROMO3, PROMO4, PROMO5, PROMO6, PROMO7
COMMON /PRTINT/ ON, IACCEL, IVEL, ITRAJ, ISIDWL, IBOWSL, IWAVES, IFAN
1RUD, IPROP, IAEROD, IRHS
COMMON /SOFTBS/ XBF, PBS, SINRS, COSBS, XBS, ZBS, DELYBS, DPBS, ELMAXB, YAVFAN
1GB(10)
COMMON /SOFTSS/ XLF, PSS, SINTH, COSTH, XSS, ZSS, DELYSS, DPSS, ELMAXS, YAVFAN
1GS(10)
COMMON /VARBLE/ VAL(40)
DIMENSION QB(1), QM(1), QS(1), PBOW(1), PM(1), PS(1), HP(8)
EQUIVALENCE (VAL(1), TIME), (VAL(2), U), (VAL(3), V), (VAL(4), W), (VAL(5), P),
1L(5), P), (VAL(6), Q), (VAL(7), R), (VAL(8), PHI), (VAL(9), THETA), (VAL(10), Z),
2L(10), Z), (VAL(11), BMASS), (VAL(21), X), (VAL(22), Y), (VAL(23), PSI)
3, (VAL(24), PB)
EQUIVALENCE (VAL(18), FANPWR)
EQUIVALENCE (QBAN(1), QB(1)), (QMFAN(1), QM(1)), (QSFAN(1), QS(1)),
1(PBFAN(1), PBOW(1)), (PMFAN(1), PM(1)), (PSFAN(1), PS(1))
DATA HP/2.9,2.3,1.95,1.77,1.85,2.05,1.93,1.62/

BRAT = 8000/BRPM
EMRAT = 8000/EMRPM
SRAT = 8000/SRPM
TL = VAL(1)
IF (NB.EQ.0.0) GO TO 1
DPBS = FGI(TL, NB, TMEB, DELB, ILB)
PBS = PB+DPBS
1 IF (NS.EQ.0.0) GO TO 2
DPSS = FGI(TL, NS, TMEB, DELS, ILS)
PSS = PB+DPSS
2 CONTINUE
PB1 = PBS-PINF
PB2 = PB-PINF
PB3 = PSS-PINF
PBARB = PB1*BRAT*BRAT
PBARM = PB2*EMRAT*EMRAT
PBARS = PB3*SRAT*SRAT
QBOW = ENBFAN*FGI(PBARB, NPTSB, PBOW, QB, IB)/BRAT
QMAIN = ENMFAN*FGI(PBARM, NPTSM, PM, QM, IM)/EMRAT
QSTN = ENSFAN*FGI(PBARS, NPTSS, PS, QS, IS)/SRAT

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C

C

FAN 10
FAN 20
FAN 30
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FAN 310
FAN 320
FAN 330
FAN 340
FAN 350
FAN 360
FAN 370
FAN 380
FAN 390
FAN 400
FAN 410
FAN 420
FAN 430
FAN 440
FAN 450


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SUBROUTINE INCON (TIME)
REAL *8 TICRD
INTEGER ON
COMMON /AIR/ PINF,RHOINF,GAM
COMMON /AXIS/ NXYS(26)
COMMON /ATRIX/ AMASSI,AIYI,DIXZ,DIZZ
COMMON /BMCO/ IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
COMMON /COLUMN/ IVERT,ILATRL
COMMON /CONST/ PI,RAD,UO
COMMON /CNTRL/ CONTW,CONTQ,CONTH,QMULT,LOUVER,ACONTZ,ACONTW,ZEQUI
COMMON /CURVE/ NCURV(10)
COMMON /ENGINE/ NPS,NPP,THSTS(25),THSTP(25),XP,YP,ZP,STHS,STHP,TIP
COMMON /EQNCO/ NEQS,TOL(20),JQQ
COMMON /FAIR/ RHOA,XLAERO
COMMON /FANMAP/ QIN,QBFAN(25),QSFAN(25),ENBFAN,ENMFAN,EN
COMMON /BRPM,EMRPM,SRPM,NPTSB,NPTSS,PBFAN(25),PSFAN(2
COMMON /DELB(25),DELB(25),NB,TMES(25),DETS(25),NS
COMMON /FROUDE/ FN,FNCRIT
COMMON /GBOW/ XBOW
COMMON /GEOM/ WIDTH,XL,XX(4,11),YY(4,11),NSTA(4),AB,VOLNOM,DELS(4,
COMMON /XCP,ZCP
COMMON /GEOMSW/ XAVG(10),DS
COMMON /GRAF/ NGRAF,NORW
COMMON /HEADG/ TICRD(6)
COMMON /PWAVE/ FNCON,PWVCON
COMMON /LEAKER/ ALEAK,BLEAK,CFSS,CFBS
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,AM
COMMON /XI(201),YI(201),ZI(201),XS,ZS,HRHO
COMMON /MATRIX/ A(6,6)
COMMON /OPTION/ I3DOF,ISRGE,ITRIM,IDIA
COMMON /PLENUM/ XLBW,XBBW,BUBHGT,DVWDOT,VMDOT,CMM
COMMON /PLVCQQ/ NVI,NVD,NLI,NLD
COMMON /PRIME/ STIME,DELTIME,DELTPNT,TPRINT
COMMON /PRINT/ ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,I
COMMON /PROP,IAEROD,IRHS
COMMON /PROMOD/ PROMOD1,PROMOD2,PROMOD3,PROMOD4,PROMOD5,PROMOD6,PROMOD7
COMMON /ROLL/ PHIMAX,TROLL
COMMON /RUDDR/ NPR,DELRUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,R
COMMON /CLB,RTC,RUDANG,TIR(25)
COMMON /RISER/ AMPTC
COMMON /SOFTBS/ XBF,PBS,SINBS,COSBS,XBS,ZBS,DELYBS,DPBS,ELMAXB,YAV
COMMON /CENCAB
COMMON /SOFTSS/ XLF,PSS,SINTH,COSTH,XSS,ZSS,DELYSS,DPSS,ELMAXS,YAV
COMMON /IGS(10)

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INCN 10
INCN 20
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INCN 330
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INCN 380
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INCN 410
INCN 420
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INCN 440
INCN 450
INCN 460
INCN 470

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COMMON /SIDE/ FXSW,FYSW,FZSW,FKSW,FMSW,FNSW,ALSW,YSW,XLSW,CFSW,CDS INCN 480
1W,VAREA,VCHORD,VSPAN,VANGLE,VCS,VX,VY,VZ,AVBMSW,DELX,VTC INCN 490
COMMON /SLOPE/ WATSLP,XPWV,XLXPWV,PWVHT,XPWVXS INCN 500
COMMON /STABLE/ S(4),ISTAB INCN 510
COMMON /STSLR/ CPHI,CPHID INCN 520
COMMON /SUM/ ISUM1(8),ISUM2(8) INCN 530
COMMON /VALOLD/ YOLD(20) INCN 540
COMMON /VARBLE/ VAL(40) INCN 550
COMMON /WAVE/ ETA(4,11),AW(20),OMEGA(20),DVOLW,NWAVE,BETA,FXWAV,FY INCN 560
1WAV,FZWAV,FKWAV,FMWAV,FNWAV,ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET,PB INCN 570
2BAR INCN 580
COMMON /WAVEF/ WAVLEN(20),OMEGAE(20),WAVSLP(20),ENCPER(20) INCN 590
COMMON /WAVTAB/ NAL,DAL,SAL,NDS,DDS,SDS,NTH,DTH,STH,NBB,DBB,SBB,AC INCN 600
11(20,5,7),AC2(20,5,7),AC3(20,5,7),AC4(20,5,7),AC5(20,5,7),AC6(20,5,7),AC INCN 610
2,7),AC7(20,5,7),AC8(20,5,7),AC9(20,5,7),AC10(20,5,7),AC11(20,5,7),AC INCN 620
3,12),AC13(20,5,7),AC14(20,5,7),AC15(20,5,7),AC16(20,5,7),AC17(20,5,7),AC INCN 630
4,18),AC19(20,5,7),AC20(20,5,7),AC21(20,5,7),AC22(20,5,7),AC23(20,5,7),AC INCN 640
5,24),AC25(20,5,7),AC26(20,5,7),AC27(20,5,7),AC28(20,5,7),AC29(20,5,7),AC INCN 650
DIMENSION ZZZ(14050) INCN 660
EQUIVALENCE (ZZZ,NAL) INCN 670
EQUIVALENCE (VAL(2),U), (VAL(3),V), (VAL(4),W), (VAL(5),P), (VAL(6) INCN 680
1),Q), (VAL(7),R), (VAL(8),PHI), (VAL(9),THETA), (VAL(10),Z), (VAL( INCN 690
211),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI), (VAL(24),PB), INCN 700
3 (VAL(12),VOL) INCN 710
DIMENSION TEMP(7), XMD(10) INCN 720
DIMENSION TITLC(20) INCN 730
DATA BEAM,BETAD,DELO,DELPI,DLRDO,DSO,ISYS,RMAXO,RONO,RRATO,RREVO,T INCN 740
1HETO,THSSI,TPRINO,UO,VXO,VZ,XBSI,XCPO,XLTO,XPO,XRO,XSSI,YPO,ZPO, INCN 750
2ZRO,ZSSI/6#0.0,0,0,20#0.0/ INCN 760
INCN 770
INCN 780
INCN 790
INCN 800
INCN 810
INCN 820
INCN 830
INCN 840
INCN 850
INCN 860
INCN 870
INCN 880
INCN 890
INCN 900
INCN 910
INCN 920
INCN 930
INCN 940
INCN 950
INITIAL CONDITIONS WITH WATSLP

DO 1 I=1,8
ISUM1(I) = 0
1 ISUM2(I) = 0

PINF = 2116.
RHOINF = .002378
GAM = 1.4
GO TO 3
2 READ (5,98) NGRAF,NDRW
READ (5,99) NXYS
READ (5,100) TICRD
3 READ (5,107) ISYSL,IOP,T,(TEMP(I),I=1,7)
IF (ISYSL.EQ. ISYS.AND. ISYSL.EQ.13) GO TO 97
ISYS = ISYSL
IF ((ISYS.LE.0).OR.(ISYS.GT.22)) GO TO 97
GO TO (4,14,23,24,27,28,31,34,37,41,42,52,53,74,75,82,89,92,93,6,7) INCN

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C
C
C

C

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1,2), ISYS
PROGRAM CONTROL PARAMETERS
4 CONTINUE
  GO TO (5,8,9,10,11,12), IOPT
5 CONTINUE
  STIME = TEMP(1)
  DELO = TEMP(2)
  DELPNT = TEMP(3)
  TPRINO = TEMP(4)
  IF (TPRINO.LT.STIME+DELPNT) TPRINO=STIME+DELPNT
  IF (DELO.GT.DELPNT) DELO=DELPNT
  IF (DELO.EQ.0.0) GO TO 13
  GO TO 3
6 READ (5,101) NCURV
7 GO TO 3
8 READ (5,102) ISUM1
  READ (5,102) ISUM2
  GO TO 3
9 READ (5,108) IACCEL, IVEL, ITRAJ, ISIDWL, IBOWSL, ISTNSL, IWAVES, IRUD, IP
  IROP, IAEROD, IRHS
  GO TO 3
10 READ (5,111) NEQS, JQQ, (TOL(J), J=1, NEQS)
  GO TO 3
11 CONTINUE
  I3DOF = TEMP(1)
  ISRGE = TEMP(2)
  ITRIM = TEMP(3)
  IDIA = TEMP(4)
  GO TO 3
12 CONTINUE
  PRCM01 = TEMP(1)
  PRCM02 = TEMP(2)
  PROM03 = TEMP(3)
  PROM04 = TEMP(4)
  PROM05 = TEMP(5)
  PROM06 = TEMP(6)
  PROM07 = TEMP(7)
  GO TO 3
13 WRITE (6,110)
  STOP
MASS DISTRIBUTION

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INCN 960
INCN 970
INCN 980
INCN 990
INCN 1000
INCN 1010
INCN 1020
INCN 1030
INCN 1040
INCN 1050
INCN 1060
INCN 1070
INCN 1080
INCN 1090
INCN 1100
INCN 1110
INCN 1120
INCN 1130
INCN 1140
INCN 1150
INCN 1160
INCN 1170
INCN 1180
INCN 1190
INCN 1200
INCN 1210
INCN 1220
INCN 1230
INCN 1240
INCN 1250
INCN 1260
INCN 1270
INCN 1280
INCN 1290
INCN 1300
INCN 1310
INCN 1320
INCN 1330
INCN 1340
INCN 1350
INCN 1360
INCN 1370
INCN 1380
INCN 1390
INCN 1400
INCN 1410
INCN 1420
INCN 1430

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14 G = 32.17
   RHO = 1.99
   HRHO = RHO*.5
   GO TO (15,17,22), IOPT
15 IMM = 0
   WEIGHT = TEMP(1)
   AM = WEIGHT/G
   XS = TEMP(2)
   ZS = TEMP(3)
   AIXX = TEMP(4)
   AIYY = TEMP(5)
   AIZZ = TEMP(6)
   AIXZ = TEMP(7)

C
C
C      INERTIA MATRIX OPERATIONS
C
16 AMASSI = 1.0/AM
   D = 1.0/(AIXX*AIZZ-AIXZ*AIXZ)
   CIXX = AIXX*D
   DIXZ = AIXZ*D
   DIZZ = AIZZ*D
   AIYYI = 1.0/AIYY
   GO TO 3

C
C
C      READ WEIGHT DISTRIBUTION - ASSUME TRANSVERSE (PORT/STBD) SYMMETRY
C      X INPUT DIST. FWD. OF (SIDEWALL) TRANSOM
C      Y INPUT DIST. TO STARBOARD
C      Z INPUT DIST. UP FROM KEEL-LINE
C
17 I = 1
18 READ (5,109) AMI(I),XI(I),YI(I),ZI(I)
   IF (AMI(I).LT.0.0) GO TO 19
   I = I+1
   IF (I.GT.201) GO TO 97
   GO TO 18
19 NMASS = I-1
   SUM = 0.0
   SUZ = 0.0
   SUZ = 0.0

C
DO 20 I=1,NMASS
   AMI(I) = AMI(I)/G
   SUM = SUM+AMI(I)
   SUZ = SUZ+AMI(I)*XI(I)
   SUZ = SUZ+AMI(I)*ZI(I)
20

C
AM = SUM*.0
WEIGHT = AM*G

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INCN1440
INCN1450
INCN1460
INCN1470
INCN1480
INCN1490
INCN1500
INCN1510
INCN1520
INCN1530
INCN1540
INCN1550
INCN1560
INCN1570
INCN1580
INCN1590
INCN1600
INCN1610
INCN1620
INCN1630
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INCN1650
INCN1660
INCN1670
INCN1680
INCN1690
INCN1700
INCN1710
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INCN1790
INCN1800
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INCN1890
INCN1900
INCN1910

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INCN 2400
 INCN 2410
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 INCN 2430
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 INCN 2500
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 INCN 2690
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 INCN 2790
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 INCN 2840
 INCN 2850
 INCN 2860
 INCN 2870

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26 CONTINUE
   GO TO 3
C
C
   STERNSEAL
27 CONTINUE
   XSSI = TEMP(1)
   ZSSI = TEMP(2)
   ALEAK = TEMP(3)
   CFSS = TEMP(4)
   FLMAXS = TEMP(5)
   DPSS = TEMP(6)
   XLF = TEMP(7)
   ARG = ELMAXS/XLF
   COSTH = ARG
   THSSI = ARCCOS(ARG)
   SINHTH = SIN(THSSI)
   GO TO 3
C
C
   BOWSEAL
28 GO TO (29,30), IOPT
29 CONTINUE
   XBSI = TEMP(1)
   CPBS = TEMP(2)
   DPBS = TEMP(3)
   ZBSI = TEMP(4)
   ELMAXB = TEMP(5)
   XBF = TEMP(6)
   BLEAK = TEMP(7)
   GO TO 3
30 CENCAB = TEMP(1)
   GO TO 3
C
C
   PLENUM
31 CONTINUE
32 GO TO (32,33), IOPT
32 CONTINUE
   XLBW = TEMP(1)
   XBBW = TEMP(2)
   XPBW = TEMP(3)
   WIDTH = TEMP(4)
   XL = TEMP(5)
   XCPD = TEMP(6)
   BUBHGT = TEMP(7)
   XLXPBW = XLBW-XPBW
   PWVHT = (XPBW*XPBW-XLXPBW)*.5/XL

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XPWVXS = XPWV-XS	INCN2880
ABW = XBBW*XLBW	INCN2890
AB = WIDTH*XL	INCN2900
VCLNOM = (ABW+AB)*BUBHGT*.5	INCN2910
GO TO 3	INCN2920
33 CONTINUE	INCN2930
FNCRIT = TEMP(1)	INCN2940
GO TO 3	INCN2950
	INCN2960
PROPULSICN	INCN2970
	INCN2980
34 CONTINUE	INCN2990
GO TO (35,36), IOPT	INCN3000
35 CONTINUE	INCN3010
XPO = TEMP(1)	INCN3020
YPO = TEMP(2)	INCN3030
ZPO = TEMP(3)	INCN3040
GO TO 3	INCN3050
	INCN3060
C BLOCK 8 OPTION 2 REMOVED. ENGINE OUT INPUT IN BLOCK 16	INCN3070
	INCN3080
36 CONTINUE	INCN3090
GO TO 3	INCN3100
	INCN3110
RUDDER	INCN3120
	INCN3130
37 CCNTINUE	INCN3140
GO TO (38,39,40), IOPT	INCN3150
38 XRO = TEMP(1)	INCN3160
YR = TEMP(2)	INCN3170
ZRO = TEMP(3)	INCN3180
RSPAN = TEMP(4)	INCN3190
RASPR = TEMP(5)	INCN3200
RAREA = TEMP(6)	INCN3210
RCLB = 2.*PI*RASPR/(RASPR+3.)	INCN3220
RTC = TEMP(7)	INCN3230
GO TO 3	INCN3240
	INCN3250
910 NOT USED	INCN3260
	INCN3270
39 CONTINUE	INCN3280
GO TO 3	INCN3290
40 CONTINUE	INCN3300
GO TO 3	INCN3310
	INCN3320
AERODYNAMICS	INCN3330
	INCN3340
41 CONTINUE	INCN3350


```

C
C
C
XLAERO = TEMP(1)
BEAM = TEMP(2)
RHOA = .5*RHOINF*XLAERO*BEAM
GO TO 3
WAVES
42 CONTINUE
IWAWSW = ICPT
IF (IWAWSW.GT.4) GO TO 97
NWAWE = TEMP(1)
IF (NWAWE.EQ.0) GO TO 3
IF (NWAWE.GT.20) GO TO 97
BETAD = TEMP(2)
BETA = BETAD/RAD
COSBET = COS(BETA)
SINBET = SIN(BETA)
TC = 1.0
GO TO (43,45,47,47), IWAWSW
C
43 DO 44 I=1,NWAWE
44 READ (5,116) OMEGA(I),AW(I)
C
C
GO TO 3
C
45 DC 46 I=1,NWAWE
46 READ (5,116) WAVLEN(I),AW(I)
C
C
GO TO 3
47 SHTWV = TEMP(3)
G1G = 32.17
G2 = G1G*G1G
G4 = G2*G2
GO TO (3,3,48,49), IWAWSW
48 CONTINUE
PERL = TEMP(4)
PERH = TEMP(5)
WNW = (2.0*3.141592)*((1.0/PERH)
WNW = (2.0*3.141592)*((1.0/PERL)
GO TO 50
49 CONTINUE
WNW = TEMP(4)
WNW = TEMP(5)
50 CONTINUE
UUU=SQRT(SHTWV*54.0)*1.6878
UU4 = UUU*UUU*UUU*UUU
CCC = (WNW/WNN)*((1./NWAWE)
WWPO = WNN

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INCEN3360
INCEN3370
INCEN3380
INCEN3390
INCEN3400
INCEN3410
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INCEN3750
INCEN3760
INCEN3770
INCEN3780
INCEN3790
INCEN3800
INCEN3810
INCEN3820
INCEN3830

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C      DO 51 I=1,NWAVE
      WWPN = WWPCC*CCC
      WW = (WWPN+WWPO)*.5
      DDW = WWPN-WWPO
      WWP0 = WWPN
      WW4 = WW*WW*WW*WW
      WW5 = WW*WW4
      SS = 0.0081*G2/(EXP(0.74*G4/(WW4*UU4))*WW5)
      OMEGA(I) = WW
      AW(I) = SQRT(2.*SS*DDW)
51 CONTINUE
C
C      GO TO 3
C
C      INITIAL CONDITIONS
C
52 CONTINUE
      UC = TEMP(1)
      THETO = TEMP(2)
      DSO = TEMP(3)
      DELPI = TEMP(4)
      DPHI = TEMP(5)
      GO TO 3
53 CONTINUE
C
C      INPUT COMPLETED. 1) PRINT ALL INPUT
      WRITE (6,123) TTITLC
      WRITE (6,124) STIME,FTIME,DELO,TPRINO,DELPNT
      WRITE (6,125) IACCEL,IVEL,ITRAJ,ISIDWL,IROWSL,ISTNSL,IWAVES,IRUD,I
1 PROP,IAEROD,I RHS
      WRITE (6,135) I3DOF,ISRGE,ITRIM,IDIA
      WRITE (6,142) PROM01,PROM02,PROM03,PROM04,PROM05,PROM06,PROM07
      WRITE (6,126) NEQS,(TOL(J),J=1,NEQS)
      WRITE (6,113) WEIGHT,XS,ZS,AIXX,AIYY,AIZZ,AIXZ
      WRITE (6,112) A,AIMAX
      WRITE (6,133) NSTA
      WRITE (6,114) YSW,XLSW,CFSW,CDSW,VANGLE,VSPAN,VCHORD,VX0,VY,VZ0,AV
1BMSW,VTC
      WRITE (6,115) NAL,DAL,SAL,NDS,DDS,SDS,NTH,DTH,STH,NBB,DBB,SBB
      IF (IMM.GT.0) WRITE (6,121) (XMD(J),J=1,IMNX)
      IF (IMNX,IMNY,IBMFIL,BTIME,IMT)
      WRITE (6,122) (YMI(J),J=1,IMNY)
      WRITE (6,128) XLBW,XBBW
      WRITE (6,129) XL,WIDTH,XCPO,VOLNOM,RUBHGT
      WRITE (6,134) DELPI
      WRITE (6,127) FNCRIT,XLTOT

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DO 60 I=1, NWAVE
WAVSLP(I) = 360.0*AW(I)/WAVLEN(I)
CMGAE(I) = 2.*PI*(SQRT(G*WAVLEN(I)/(2.*PI)) - U*COSBET)/WAVLEN(I)
ENCPER(I) = 2.0*PI/OMEGAE(I)
60 CONTINUE
C
WRITE (6,117) NWAVE, BETAD, (OMEGA(I), OMEGAE(I), WAVLEN(I), AW(I), WAVS
1LP(I), ENCPER(I), I=1, NWAVE)
GO TO 62
61 WRITE (6,118)
62 CONTINUE
C
DO 63 I=1, 4
DO 63 N=1, 11
ETA(I, N) = 0.0
C
DVOLW = 0.0
FXWAV = 0.0
FYWAV = 0.0
FZWAV = 0.0
FKWAV = 0.0
FMWAV = 0.0
FNWAV = 0.0
ZBAR = Z
PHIBAR = PHI
THEBAR = THE TA
TIME = TIME
DELT = DELC
TPRINT = TPRINO-DELPNT
PWVCON = 4.*WEIGHT/(RHO*G*XLBW)
FNCON = SQRT(XLBW*G)
VX = VX0-XS
VZ = ZS-VZ0
XP = XPO-XS
XR = XRO-XS
YP = YPO
ZP = ZS-ZPO
ZR = ZS-ZRO
IF (IMM.EQ.0) GO TO 65
C
DO 64 J=1, IMNX
XMI(J) = XMO(J)-XS
64 CONTINUE
C
XCP = XCP0-XS
ZCP = ZS-BUBHGT
XBS = XBSI-XS
65 CONTINUE

```

```

C      N = NSTA(3)
      ZBS = ZS-ZBSI
      DO 66 J=1,N
      DELYBS = XBBW/(N-1)
      XX(3,J) = XBS-XSSI
      YY(3,J) = -0.5*XBBW+(J-1)*DELYBS
66      CONTINUE
C
C      N = N-1
      DO 67 J=1,N
      YAVGB(J) = (YY(3,J+1)+YY(3,J))*0.5
67      CONTINUE
C
C      N = NSTA(4)
      DELYSS = XBBW/(N-1)
      DO 68 J=1,N
      XX(4,J) = -XS
      YY(4,J) = -0.5*XBBW+(J-1)*DELYSS
68      CONTINUE
C
C      N = N-1
      DO 69 J=1,N
      YAVGS(J) = (YY(4,J+1)+YY(4,J))*0.5
69      CONTINUE
C
      XBOW = XLTOT-XS
      N = NSTA(1)
      DELX = XBSI/(N-1)
      DO 70 J=1,2
      DO 70 I=1,N
      XX(J,I) = (I-1)*DELX-XS
      YY(J,I) = YSW*(2*J-3)
70      WRITE (6,103) ((XX(J,N),N=1,11),(YY(J,N),N=1,11),J=1,4)
      N = NSTA(1)-1
C
      DO 71 I=1,N
      XAVG(I) = DELX*(2*I-1)*0.5-XS
71      CALL WAVES (TIME)
C
C
C

```

```

INCN5280
INCN5290
INCN5300
INCN5310
INCN5320
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INCN5340
INCN5350
INCN5360
INCN5370
INCN5380
INCN5390
INCN5400
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INCN5650
INCN5660
INCN5670
INCN5680
INCN5690
INCN5700
INCN5710
INCN5720
INCN5730
INCN5740
INCN5750

```


C INITIALIZE BUBBLE PRESSURE, ABSOLUTE (PSF)

PB = PINF+DELPI
 PBBAR = DELPI
 PBAR = DELPI
 PSS = PB+DPSS
 PBS = PB+DPBS
 AB = ARW-(ARW-AB)*(ZS+Z/8UBHGT)
 CF = .37/((U/FNCON)**1.5655981)
 WATSLP = PBBAR*CF*PWVCN/WEIGHT
 IF (IDIA.EQ.1) GO TO 72
 VOL = VOLNOM-.5*(AB+ABW)*(Z+ZS)-DVOLW+.5*WATSLP*XL*AB
 GO TO 73

72 VOL = VOLNOM-.5*(AB+ABW)*(Z+ZS)-DVOLW+PBAR*.3175+.5*WATSLP*XL*AB
 73 CONTINUE = (PB/PINF)**(1./GAM)*VOL*RHOINF
 BMASS = (PB/PINF)**(1./GAM)*VOL*RHOINF
 WRITE (6,137)
 DVWDOT = 0.0
 RETURN

C RUN TERMINATOR

74 WRITE (6,106)
 STOP

C BENDING MOMENT

75 GO TO (76,77,79,81), IOPT
 76 IMM = TEMP(1) GO TO 97
 IF (IMM.GT.3) GO TO 97
 IMNX = TEMP(2)
 IF (IMNX.GT.10) GO TO 97
 IMNY = TEMP(3)
 IF (IMNY.GT.7) GO TO 97
 IBMFIL = TEMP(4)
 BTIME = TEMP(5)
 IF (IMM.EQ.3) IMT = TEMP(6)
 GO TO 3

77 DO 78 J=1,7
 78 XMO(J) = TEMP(J)

IF (IMNX.LE.7) GO TO 3
 READ 120, (XMO(J),J=8,IMNX)
 GO TO 3

79 DO 80 J=1,IMNY
 80 YMI(J) = TEMP(J)

INCN5760
 INCN5770
 INCN5780
 INCN5790
 INCN5800
 INCN5810
 INCN5820
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 INCN5980
 INCN5990
 INCN6000
 INCN6010
 INCN6020
 INCN6030
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 INCN6090
 INCN6100
 INCN6110
 INCN6120
 INCN6130
 INCN6140
 INCN6150
 INCN6160
 INCN6170
 INCN6180
 INCN6190
 INCN6200
 INCN6210
 INCN6220
 INCN6230


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C      GO TO 3
      81 CONTINUE
      GO TO 3
      82 CONTINUE
      GO TO (83,85,87), IOPT
      83 CONTINUE
C      VALUES INPUT FOR STBD SCREW
C
      THST1 = TEMP(1)
      NPS = TEMP(2)
      STHS = TEMP(3)
      IF (NPS.EQ.0.0) GO TO 84
      READ (5,104) (TIS(J),J=1,NPS)
      GO TO 3
      84 THSTS(1) = THST1
      85 CONTINUE
C      VALUES INPUT FOR PORT SCREW
C
      THST2 = TEMP(1)
      NPP = TEMP(2)
      STHP = TEMP(3)
      IF (NPP.EQ.0.0) GO TO 86
      READ (5,104) (TIP(J),J=1,NPP)
      READ (5,104) (THSTP(J),J=1,NPP)
      GO TO 3
      86 THSTP(1) = THST2
      87 CONTINUE
C      VALUES INPUT FOR RUDDER
C
      DELR = TEMP(1)
      NPR = TEMP(2)
      IF (NPR.EQ.0.0) GO TO 88
      READ (5,104) (TIR(J),J=1,NPR)
      READ (5,104) (DELRUD(J),J=1,NPR)
      GO TO 3
      88 DELRUD(1) = DELR
      GO TO 3
      89 GO TO (90,91), IOPT
      90 NB = TEMP(1)
      READ (5,104) (TMEB(I),I=1,NR)
      READ (5,104) (DELB(I),I=1,NB)
      GO TO 3
      91 NS = TEMP(1)

```

```

C      READ (5,104) (TMES(I),I=1,NS)
C      READ (5,104) (DETS(I),I=1,NS)
C      GO TO 3
C
C      TITLE CARD (ALL 80 COLUMNS )
C
C      92 READ (5,136) TITLC
C      GO TO 3
C
C      FAN MAPS
C
C      93 CONTINUE
C      GO TO (94,95,96), IOPT
C
C      94 CONTINUE
C      ENBFAN = TEMP(1)
C      BRPM = TEMP(2)
C      NPSTB = TEMP(3)
C      READIN = TEMP(4)
C      IF (READIN.EQ.0.0) GO TO 3
C      READ (5,104) (PBFFAN(J),J=1,NPTSB)
C      READ (5,104) (QBFFAN(J),J=1,NPTSB)
C      GO TO 3
C
C      95 CONTINUE
C      ENMFAN = TEMP(1)
C      EMRPM = TEMP(2)
C      NPSTSM = TEMP(3)
C      READIN = TEMP(4)
C      IF (READIN.EQ.0.0) GO TO 3
C      READ (5,104) (PMFFAN(J),J=1,NPTSM)
C      READ (5,104) (QMFFAN(J),J=1,NPTSM)
C      GO TO 3
C
C      96 CONTINUE
C      ENSFAN = TEMP(1)
C      SRPM = TEMP(2)
C      NPSTSS = TEMP(3)
C      READIN = TEMP(4)
C      IF (READIN.EQ.0.0) GO TO 3
C      READ (5,104) (PSFFAN(J),J=1,NPTSS)
C      READ (5,104) (QSFFAN(J),J=1,NPTSS)
C      GO TO 3
C
C      ERROR IN INPUT
C
C
C      97 CONTINUE
C      WRITE (6,105) ISYS
C      STOP
C
C

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INCN6720
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98 FORMAT (2I2)
99 FORMAT (26I2)
100 FORMAT (6A8)
101 FORMAT (10I1)
102 FORMAT (8I2)
103 FORMAT (//17H XX AND YY ARRAYS/14H PORT SIDEWALL/2(11F10.2/),15H SIDEWALL/2(11F10.2/),9H BOW SEAL/2(11F10.2/),11H STERN SEAL/2(11F10.2/))
104 FORMAT (8F10.0)
105 FORMAT (34H INPUT ERROR - - - STOP - - - ISYS=,I3)
106 FORMAT (1H1,20(/),50X,19H COMPLETED ALL RUNS)
107 FORMAT (13I2,7F10.0)
108 FORMAT (16I5)
109 FORMAT (5F10.0)
110 FORMAT (//10X,65HERROR IN INPUT --- DELT AND/OR DELPNT EQUALS ZERO)
111 FORMAT (2I2/(8F10.0))
112 FORMAT (22H INERTIA MATRIX, AIMAX6E15.4/(22X,6F15.4))
113 FORMAT (30H WEIGHT, C.G., INERTIA MOMENTS7F12.3)
114 FORMAT (15H SIDEWALL INPUT12(F8.3,1X))
115 FORMAT (26H SIDEWALL TABLE PARAMETERS4(I4,F7.3,F7.3))
116 FORMAT (2F10.0)
117 FORMAT (//12HONO OF WAVES12,10H BETA(DEG)F5.0/15H OMEGA(RAD/SEC),5X)
118 FORMAT (1,16H OMEGA(RAD/SEC)5X,16H WAVE LENGTH(FT)5X,14H AMPLITUDE(FT)5X,1)
119 FORMAT (26HMAX SLOPE (DEG)5X,13HPERIOD,E (SEC)/(F8.4,12X,F8.4,4F20.3))
120 FORMAT (32HOMOMENT CALC. CONTROL PARAMETERS4I5,F8.3,I5)
121 FORMAT (5X,7F10.0)
122 FORMAT (22H MOMENT CALCS. AT X OF11F10.3)
123 FORMAT (22H MOMENT CALCS. AT Y OF11F10.3)
124 FORMAT (33H1 SES MOTIONS AND LOADS PROGRAM - 20A4,/ )
125 FORMAT (23H START AND FINISH TIMES2F10.2/22H INITIAL TIME INTERVAL)
126 FORMAT (1F12.4/18H START PRINTING ATF8.2,17H IN INCREMENTS QFF8.2)
127 FORMAT (24H INTERMEDIATE PRINT TAGS16I5)
128 FORMAT (39H NO. OF STATE EQUATIONS, AND TOLERANCESI5/(10X,10E12.2))
129 FORMAT (23HOCRITICAL FROUDE NUMBERF15.4,5X,19H TOTAL CRAFT LENGTH)
130 FORMAT (15.4)
131 FORMAT (34HOPLENUM, LENGTH AND WIDTH AT WATER2F12.4)
132 FORMAT (34H PLENUM, LENGTH AND WIDTH AT HULL 2F12.4/35H PLENUM, CF)
133 FORMAT (INTER OF PRESSURE AT HULLF12.4/23H PLENUM, NOMINAL VOLUMEF12.1,10X, )
134 FORMAT (26HHEIGHTF12.4)
135 FORMAT (/33H PROPULSION, X, Y, Z COORDINATES 3F12.4/)
136 FORMAT (/28HORUDDER, X, Y, Z COORDINATES3F12.4/41H RUDDER, ON, MAX)
137 FORMAT (1, RATE, REVERSE, INITIAL 5F12.4/33H RUDDER, SPAN, ASPECT, AREA, CLB, T/ )
138 FORMAT (2C 5F12.4)
139 FORMAT (/39HONINITIAL CONDITIONS, VELOCITY (KNOTS) =F7.2,5X,13HPITC)
140 FORMAT (1H (DEG) =F8.3,5X,12HDRAFT (IN) =F8.2)

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133 FORMAT (49H NUMBER OF STATIONS, SIDEWALLS (P+S), SEALS (B+S),4I5) INCN7680
134 FORMAT (38H PLENUM, INITIAL PRESSURE, GAGE (PSF) F8.2) INCN7690
135 FORMAT (79H PROGRAM OPTION SWITCH SETTINGS (LATERAL PLANE, CONSTANT INCN7700
1 SPEED, TRIM, MEMBRANE) 7I5) INCN7710
136 FORMAT (20A4) INCN7720
137 FORMAT (1H1) STERNSEAL INPUT7F12.4) INCN7730
138 FORMAT (16H BOWSEAL INPUT 7F12.4) INCN7740
139 FORMAT (16H BOWSEAL INPUT7F12.4) INCN7750
140 FORMAT (19H0AERODYNAMICS INPUT7F12.4) INCN7760
141 FORMAT (33H0FANS, NO. + RPM, BOW, MAIN, STERN 3(F10.0,F10.1)) INCN7770
142 FORMAT (32H PROGRAM MODIFICATION SETTINGS 7(F12.4,1X)) INCN7780
END INCN7790

SUBROUTINE INTGRL (TIME)
INTEGER CN
COMMON /AIR/ PINF,RHOINF,GAM
COMMON /BMCO/ IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
COMMON /EQNCO/ NFQS,TOL(20),JQQ
COMMON /KSWTCH/ ITHRST
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,AM
1 I(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO
COMMON /OPTION/ I3DOF,ISRGE,ITRIM,IDA
COMMON /PLENUM/ XLBW,XBRW,ARW,BUBHGT,DVWDOOT,VMDOT,PMDOT
COMMON /PRIME/ STIME,FTIME,DELT,DELPNT,IPRINT
COMMON /PROMOD/ PROMOD1,PROMOD2,PROMOD3,PROMOD4,PROMOD5,PROMOD6,PROMOD7
COMMON /PRTINT/ ON,IACCEL,IVFL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,I
1 IRUD,IPROP,IAEROD,IRHS
COMMON /STABLE/ S(4),ISTAB
COMMON /STEP/ STEP2
COMMON /VALOLD/ YOLD(20)
COMMON /VARBLE/ VAL(40)
EQUIVALENCE (VAL(1),X), (VAL(2),Y(1))
DIMENSION Y(20), ERROR(20)
REAL K1(20),K2(20),K3(20),K4(20),K5(20)
CATA IPASS/0/
STEP2 = 1.0
PB = VAL(24)
BMASS = VAL(10)
IF ((TIME+DELT).LE.TPRINT) GO TO 1
DELT = DELT
DEL T = TPRINT-TIME
IPASS = 1
1 X = TIME
C
DO 2 J=1,NEQS
Y(J) = YOLD(J)
2 CONTINUE
C

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2L(10),Z), (VAL(11),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI) PROP 160
3, (VAL(24),PB) PROP 170
DIMENSION THS(1), THP(1), TS(1), TP(1), RUD(1), TR(1) PROP 180
EQUIVALENCE (THS(1),THS(1)), (THSTP(1),THP(1)), (TIS(1),TS(1)), PROP 190
1(TIP(1),TP(1)), (TIR(1),TR(1)), (DELRUD(1),RUD(1)) PROP 200
FX = 0.0 PROP 210
FY = 0.0 PROP 220
FZ = 0.0 PROP 230
FK = 0.0 PROP 240
FM = 0.0 PROP 250
FN = 0.0 PROP 260
TL = TIME PROP 270
IF (NPR.EQ.0.0) GO TO 1 PROP 280
RUDANG = FGI(TL,NPR,TR,RUD,IR) PROP 290
RUCANG = RUDANG/RAD PROP 300
PROP 310
PROP 320
C CALCULATE THRUSTS AND MOMENTS INDIVIDUALLY
C
C
GO TO 2
1 RUDANG = DELRUD(1) PROP 330
2 CD = CCS(RUDANG) PROP 340
SD = SIN(RUDANG) PROP 350
IF (NPS.EQ.0.0) GO TO 3 PROP 360
THSS = FGI(TL,NPS,TS,THS,IS) PROP 370
GO TO 4 PROP 380
3 THSS = THSTS(1) PROP 390
4 THSP = FGI(TL,NPP,TP,THP,IP) PROP 400
GO TO 6 PROP 410
5 THSP = THSTP(1) PROP 420
6 STHSTP = STHP*THSP PROP 430
FXS = THSS*CD-STHSTS*SD PROP 440
FXP = THSP*CD+STHSTP*SD PROP 450
FYS = -STHSTS*CD-THSS*SD PROP 460
FZS = -THSS*THETA*CD+STHSTS*SD*PHI PROP 470
FZP = -THSP*THETA*CD-STHSTP*SD*PHI PROP 480
FX = FXP+FXS PROP 490
FY = FYP+FYS PROP 500
FZ = FZP+FZS PROP 510
FKP = -FZP*YP-FYP*ZP PROP 520
FKS = FZS*YP-FYS*ZP PROP 530
FK = FKS+FKP PROP 540
FMS = FZS*(-XP)+FXS*ZP PROP 550
FMP = FZP*(-XP)+FYP*ZP PROP 560
PROP 570
PROP 580
PROP 590
PROP 600
PROP 610
PROP 620
PROP 630

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C

C
C

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FM = FMS+FMP
FNS = -FXS*YP-FYS*(-XP)
FNP = FXP*YP-FYP*(-XP)
FN = FNS+FNP
IF (I PROP.NE.ON) RETURN
WRITE (6,7) FX,FY,FZ,FK,FM,FN
RETURN

7 FORMAT (/10X,22HPPOP FX,FY,FZ,FK,FM,FN/6F15.4)
END

SUBROUTINE RUDDER

INTEGER CN
COMMON /CONST/ PI,RAD,UO
COMMON /FRUD/ FX,FY,FZ,FK,FM,FN
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,AMRUD
11(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO
COMMON /PROMOD/ PROMO1,PROMO2,PROMO3,PROMO4,PROMO5,PROMO6,PROMO7
COMMON /PRTINT/ ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,IRUD
1RUD,IPROP,IAEROD,IRHS
COMMON /RUDDR/ NPR,DEL RUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,R
1CLB,RTC,RUDANG,TIR(25)
COMMON /VARBLE/ VAL(40)
EQUIVALENCE (VAL(1),TIME), (VAL(2),U), (VAL(3),V), (VAL(4),W), (VARUD
1L(5),P), (VAL(6),Q), (VAL(7),R), (VAL(8),PHI), (VAL(9),THETA), (VARUD
2L(10),Z), (VAL(11),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI)
3, (VAL(24),PB)
EQUIVALENCE (DELPUD(1),RUD(1)), (TIR(1),TR(1))
DIMENSION RUD(1), TR(1)
EQUIVALENCE (VAL(18),FANPWR)
DATA ENU/1.28E-5/

CALCULATE PROGRAMMED RUDDER DEFLECTION

TL = TIME
IF (NPR.EQ.0.0) GO TO 1
GO TO 2
1 RUDANG = DELRUD(1)
RUDANG = RUDANG/RAD
GO TO 3
2 RUDANG = FGI(TL,NPR,TR,RUD,IR)
RUDANG = RUDANG/RAD

SIDE FORCE ON RUDDER

3 DSR = Z+ZS-XR*THETA
ENDFAC = (1.+DSR/(DSR+RSPAN))

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COMMON /GEOMBS/ DETABX(11),DETABT(11),ARM1B(10),ARM2B(10),DFBS(10)RHS
1,TSKIE(10)RHS
COMMON /GEOMSS/ DETADX(11),DETADT(11),ARM1S(10),DFSS(10),TSKIS(10)RHS
1,ARM2S(10)RHS
COMMON /KSWTCH/ ITHRST
COMMON /MASSES/ AM,AIXX,AIYZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,AMRHS
1I(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO
COMMON /MSIDW/ DF(2,10),DSWAV(2,10),FXH(2),FYH(2),FZH(2),FMH(2),FNRHS
1H(2),VFY(2),VFZ(2),FXV
COMMON /MWAVE/ FXW(2),FYW(2),FKW(2),FMW(2),FNW(2)
COMMON /OPTION/ I3DOF,ISRGE,ITRIM,IDI
COMMON /PLENUM/ XLBW,XBBW,ABW,BUBHGT,DVWDOT,VMDOT,CM
COMMON /PRIME/ STIME,DELTIME,DELTPNT,TPRINT
COMMON /PRINT/ ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,IRHS
1RUD,IPROP,IAEKOD,IRHS
COMMON /PROMOD/ PROMO1,PROMO2,PROMO3,PROMO4,PROMO5,PROMO6,PROMO7
COMMON /PWAVE/ FNCON,PWVCON
COMMON /RUDDR/ NPR,DELKUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,RHS
1CLB,RTC,RUDANG,TIR(25)
COMMON /SIDE/ FXSW,FYSW,FZSW,FKSW,FMSW,FNSW,ALSW,YSW,XLSW,CFSW,CDSRHS
1W,VAREA,VCHORD,VSPAN,VANGLE,VCONS,VX,VY,VZ,AVBMSW,DELX,VTC
COMMON /SLOPE/ WATSLP,XPWV,XLX2,PWVHT,XPWVXS
COMMON /SOFTBS/ XBF,PBS,SINBS,COSBS,XBS,ZBS,DELYBS,DPBS,ELMAXB,YAVRHS
1GB(10),CENCAB
COMMON /SOFTSS/ XLF,PSS,SINTH,COSTH,XSS,ZSS,DELYSS,DPSS,ELMAXS,YAVRHS
1GS(10)
COMMON /VALOLD/ YOLD(20)
COMMON /VARBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(20),OMEGA(20),DVOLW,NWAVE,BETA,FXWAV,FYRHS
1WAV,FZWAV,FKWAV,FMWAV,FNWAV,ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET,PBRHS
2BAR
EQUIVALENCE (VAL(1),TIME), (VAL(2),U), (VAL(3),V), (VAL(4),W), (VARHS
1L(5),P), (VAL(6),Q), (VAL(7),R), (VAL(8),PHI), (VAL(9),THETA), (VARHS
2L(10),Z), (VAL(11),RMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI)RHS
3, (VAL(24),PB)
EQUIVALENCE (VAL(18),FANPWR)
DIMENSION ACCEL(3), ANGACL(3)
DIMENSION GF(6), VALUE(20)
DATA CCF/4.9E-07/

DO 1 J=1,20
1 VALUE(J) = 0.0

CALCULATION OF BUBBLE WAVE MAKING DRAG

AB = ABW-(ABW-(XL*WIDTH))*(ZS+Z)/BUBHGT

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CC

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CC


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FN = U/FNCON
CF = .37/(FN**1.5655981)
FXPWAV = -PWVCON*PBAR*CF
WATSLP = -FXPWAV/WEIGHT
VOL = VAL(12)
PB = VAL(13)
PBAR = VAL(13)-PINF
PBS = PB+DPBS
PSS = PB+DPSS
ABPB = PBAR*AB
CALCULATION OF BUBBLE WAVE MAKING DRAG
FLOW = SQR(2.*ABS(PBAR)/RHOINF)*SIGN(1.,PBAR)
GLSW = CFSW*ALSW*FLOW
CALL BOWSL
CALL STNSL
SUMX = FXBS+FXSS+FXSW+FXRUD+FXP+FXWAV+FXAED+FXPWAV
IF (ITHRST.NE.ITRIM) GO TO 2
THSTS(1) = THSTS(1)-SUMX*.5
THSTP(1) = THSTP(1)-SUMX*.5
THST = THSTS(1)+THSTP(1)
SUMX = 0.0
CONTINUE
SUMY = FYBS+FYSS+FYSW+FYRUD+FYP+FYWAV+FYAED
SUMZ = WEIGHT-ABPB+FZBS+FZSS+FZSW+FZRJD+FZP+FZWAV+FZAED
SUMK = FKBS+FKSS+FKSW+FKRUD+FKP+FKWAV+FKAED+ABPB*PHI*(-Z)
CALCULATION OF EFFECTIVE CENTER OF PRESSURE
UU = U*0.5921-30.0
XCPU = XCP+0.001975*UU*UU-0.974
XCPC = SHXYAX(XCPU,ZCP,THETA,PI)
FMBUB = ABPB*XCPC
SUMM = FMBBS+FMSS+FMWS+FMRUD+FMP+FMWAV+FMAED+FMBUB+FXPWAV*ZS
FWAVZ = FXPWAV*ZS
SUMN = FNBBS+FNSS+FNWS+FNURUD+FNP+FNWAV+FNAED
IF (I3DOF.NE.1) GO TO 3
SUMZ = 0.0
SUMM = 0.0
CONTINUE
VALUE(1) = SUMX*AMASSI
VALUE(2) = SUMY*AMASSI-R*U
VALUE(3) = SUMZ*AMASSI
VALUE(4) = SUMK*DIXZ+SUMN*DIXZ
VALUE(5) = SUMM*AIYYI
VALUE(6) = SUMN*DIXX+SUMK*DIXZ

```

C C

C

C

2

C C

3

```

VALUE(7) = P
VALUE(8) = Q
VALUE(9) = W
IF (I3COF.EQ.1) GO TO 6
BUBBLE PRESSURE EQUATION
GOUT = QLBS+QLSS+QLSW
CALL FAN
VALUE(10) = RHOINF*(QIN-QOUT)
VALUE(11) = -(((XL*WIDTH)+ABW)*.5)*W-DVWDOT
VALUE(12) = VAL(13)*GAM*((VALUE(10)/VAL(11))-(VALUE(11)/VAL(12)))
IF (IDIA.EQ.1) GO TO 4
GO TO 5
4 CONTINUE
MEMBRANE STUDY
VAL(12)=VAL(12)+0.3175*VAL(13)
VAL(12)=VAL(13)*GAM*((VALUE(10)/VAL(11))-(VALUE(11)/VAL(12)))
5 CONTINUE
GO TO 7
6 CONTINUE
VALUE(10) = 0.0
7 CONTINUE
WRITE DATA FILE FOR MOMENT AND SHEAR CALCS., IF REQUIRED
IF (IMT.NE.1) GO TO 8
NBS = NSTA(3)-1
NSS = NSTA(4)-1
NSSL = NSS/2+1
WRITE (IBMFIL) (VAL(I),I=1,24),ZBAR,PHIBAR,THEBAR,FXW,FYW,FZW,FKW,FXV,
1FMW,FNW,(VALUE(I),I=1,10),DE,DSWAV,FXH,FYH,FZH,FMH,FNH,VFZ,FXV,
2,FXRUD,FYRUD,FXP,FYP,FZP,FZSS,FKSS,FMSS,FXBS,FZBS,FXAED,FYAED,FZAE,
3D,FMAED,FNAED,FXPWA,FXSS,FKBS,FMBS,FNBS,(TSKIS(I),I=1,NBS),
4NSSL,NSS),(TSKIB(I),DFBS(I),ARM1B(I),ARM2B(I),I=1,NBS)
8 CONTINUE
CONSTANT LONGITUDINAL VFLOCITY ( U )
IF (ISRGE.EQ.1) VALUE(1)=0.0
IF (ON.NE.1) RETURN
DO 9 I=1,3
ACCEL(I) = VALUE(I)/G
ANGACL(I) = VALUE(I+3)*RAD

```



```

9 CONTINUE
  BOWACC = ACCEL(3)-XBOW*VALUE(5)/G
  STNACC = ACCEL(3)+XS*VALUE(5)/G
  IF (IVERT.NE.ON) GO TO 10
  ZD = Z+ZS
  VOLP = VCL
  THETAR = THETA*RAD
  QDEG = Q*RAD
10 IF (ILATRL.NE.ON) GO TO 13
  DEPSI = PSI*RAD
  PDEG = P*RAD
  RDEG = R*RAD
  BETAS = -V/U*RAD
  ACCLAT = (VALUE(2)+U*R)/G
  DPHI = PHI*RAD
  DRFT = 12.0*ZD
  VEL = 0.5925*U
  DELRS = RUDANG*RAD
  IF (R.EQ.0.0) GO TO 11
  TRADUS = U/R
  GO TO 12
11 TRADUS = 1.E8
12 WRITE (1) TIME, VAL(16), DRFT, THETAR, PBAR, BOWACC, ACCEL(3), FANPWR, DPHRHS
13 IF (IRHS.NE.ON) RETURN
  FMSW, FMSS, FMRUD, FMP, FMWAV, FMAED, FMRUB, FWAVZ
  WRITE (6,14)
  WRITE (6,15) EXPWAV
  WRITE (6,16) PBAR, FANPWR, QIN, QLBS, GLSW, QLSS
  WRITE (6,17) AP, VOL
  WRITE (6,18) VALUE, VAL
  WRITE (6,19) GF, ACCEL, ANGACL
  WRITE (6,20) BOWACC, STNACC
  RETURN
14 FORMAT ('0', 6X, 5HFMBSS=, E16.6, 2X, 5HFMRUD=, E16.6, 2X, 5HFMSW=,
1  E16.6, /, '0', 6X, 6HFMAED=, E16.6, 2X, 4HFMP=, E16.6, 2X, 6HFMMWAV=, E16.6,
2  /, '0', 6X, 6HFMAED=, E16.6, 2X, 6HFMRUB=, E16.6, 2X, 6HFMAVZ=, E16.6)
15 FORMAT ('0', 6X, 7HFEXPWAV=, E16.6)
16 FORMAT (/ / 10X, 3HPHS2OHGAGEPRESS. (PSF)=F7.2, 5X, 21HFAN POWER REQD (HRS
1P)=F8.2, 5X, 27HFAN FLOW RATE (CU FT/SEC) =F9.2, / / 31H LEAKAGE FLOW
2RATES (CU FT/SEC) / / 11H BOW SEAL =F9.2, 11H SIDEWALL =F9.2, 13H STERN
3 SEAL =F9.2)
17 FORMAT (/ / 13H PLENUM AREA=F9.2, 10X, 14HPLENUM VOLUME=F10.2)
18 FORMAT (/ / 12H VALUE ARRAY2(/10E13.4) / 10H VAL ARRAY4(/10E13.4))

```

RHS 1690
 RHS 1700
 RHS 1710
 RHS 1720
 RHS 1730
 RHS 1740
 RHS 1750
 RHS 1760
 RHS 1770
 RHS 1780
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 RHS 2040
 RHS 2050
 RHS 2060
 RHS 2070
 RHS 2080
 RHS 2090
 RHS 2100
 RHS 2110
 RHS 2120
 RHS 2130
 RHS 2140
 RHS 2150
 RHS 2160


```

211),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI), (VAL(24),PB)
DIMENSION GAP(2,11), DSW(2,11)
DIMENSION FZHO(2), FZHDRP(2)
DATA ENU/1.28E-5/
PBAR = PB-PINF
PBHEAD = PBAR/(RHO*G)
GAP OR WETTED DRAFT CALCULATION
DO 5 J=1,2
N = NSTA(J)
DO 5 K=1,N
DD = ZS+Z+YY(J,K)*PHI-XX(1,K)*THETA+ETA(J,K)
DDIN = DD-WATSLP*(XPWVXS-XX(J,K))
IF (DDIN.LT.BUBHGT) GO TO 1
IF (VAL(1)-TOLD.LT.DELPNT) GO TO 1
TOLD = VAL(1)
WRITE (6,14) XX(J,K), VAL(1),DD
1 CONTINUE
DSW(J,K) = (SIGN(1.,DD)+1.)*DD/2.
IF (DDIN) 2,4,4
2 IF (DSW(J,K)-PBHEAD) 3,4,4
3 GAP(J,K) = -DDIN*(1.-(DSW(J,K))/PBHEAD)
GO TO 5
4 GAP(J,K) = 0.0
5 CONTINUE
LEAKAGE AREA
ALSW = 0.0
DO 6 J=1,2
N = NSTA(J)-1
DO 6 I=1,N
ALSW = ALSW+(GAP(J,I)+GAP(J,I+1))*DELX/2.
6 CONTINUE
CROSS-FLOW DRAG ON SIDEWALLS
FYD = 0.0
FKD = 0.0
FND = 0.0

```

```

C      DO 7 I=1,2
C      N = NSTA(I)-1
C
C      DO 7 J=1,N
C      DSWAV(I,J) = (DSW(I,J)+DSW(I,J+1))/2.
C      VREL = V+XAVG(J)*R-({ZS-DSWAV(I,J)/2.})*P
C      DF(I,J) = -HRHO*CDSW*VREL*ABS(VREL)*DELX*DSWAV(I,J)
C      FYD = FYD+DF(I,J)
C      FND = FND+DF(I,J)*XAVG(J)
C      7 FKD = FKD-(ZS-DSWAV(I,J)/2.)*DF(I,J)
C
C      SET UP STERN LIMIT OF FORCE DETERMINATION
C
C      XSS = -XS
C      GO TO 8
C      ENTRY SIDWLM
C      XSS = XMI(IX)
C      8 IP = 1+(THETA*PAD-STH)/DTH
C      IP = MAXO(MINO(IP,NTH),1)
C      IPL = MINO(IP+1,NTH)
C      DTHETA = (IP-1)*DTH+STH
C      DIP = (THETA*RAD-DTHETA)/DTH
C
C      CALC REYNOLDS NO. AND DRAG COEFF.
C
C      REY = U*XLSW/ENU
C      CDT = .427/(ALOG10(REY)-.407)**2.64
C
C      SIDEWALL FORCES, P/S
C
C      DO 11 J=1,2
C      WAREA = 0.0
C      N = NSTA(J)-1
C      NI = (XSS+XS)*N/XLSW+1.5
C
C      DO 9 I=NI,N
C      ZORI = 1.
C      IF (DSWAV(J,I).EQ.0.0) ZORI=0.0
C      9 WAREA = WAREA+DELX*(2.*DSWAV(J,I)+ZORI*AVBMSW)
C
C      FXH(J) = -HRHO*CDT*WAREA*U*U
C      FM1 = 2*J-3
C      YLSW = PM1*YSW
C      DSS = Z+ZS+YLSW*PHI
C      DSS = DS-XSS*THETA

```



```

ZORI = (SIGN(1.,DSS)+1.)*0.5
DSS = DSS*ZORI
IDSS = 1.5+(DSS-SBB)/DBB
IDSS = MINO(NBB,IDSS)
BS = BB(IDSS)
ZORI = (SIGN(1.,DSS)+1.)*0.5
DSS = DSS*ZORI
DRBOW = DSS-(XX(J,N+1)-XSS)*THETA
IF (DRBOW.LT.0.0) DRBOW=0.0
A33S = (RHO*PI*BS**2)*0.125
A22S = (RHO*.4*PI*DSS**2)*0.5
IF (THETA.LT.0.0) A22S=.4*RHO*PI*DRBOW*DRBOW*0.5
DSR = DS-(XREF-XS)*THETA
ID = 1.+(DSR*12.-SDS)/FDS
ID = MAXO(MINO(ID,NDS),1)
DDSR = (ID-1)*DDS+SDS
IDI = MINO(ID+1,NDS)
DID = (DSR*12.-DDSP)/DDS
BCO = ACO(1,ID,IP)
BCO0 = ACO(1,ID,IP)
BC2 = AC2(1,ID,IP)
BC5 = AC5(1,ID,IP)
BC6 = AC6(1,ID,IP)
BCO = BCO+DID*(ACO(1,ID1,IP)-BCO)+DIP*(ACO(1,ID,IP1)-BCO(1,ID,IP1)+BCO)
BCO0 = BCO0+DID*(ACO(1,ID,IP1)-BCO(1,ID1,IP1)-BCO0)+DIP*(ACO(1,ID,IP1)+BCO0)
BC2 = BC2+DID*(AC2(1,ID,IP1)-BC2)+DIP*(AC2(1,ID1,IP1)+BC2)
BC5 = BC5+DID*(AC5(1,ID,IP1)-BC5)+DIP*(AC5(1,ID1,IP1)+BC5)
BC6 = BC6+DID*(AC6(1,ID,IP1)-BC6)+DIP*(AC6(1,ID1,IP1)+BC6)
11,ID1,IP1) = BC0+DID*(ACO(1,ID,IP1)-BC0)+DIP*(ACO(1,ID,IP1)-BC0(1,ID,IP1)+BCO)
1*(ACO(1,ID1,IP1)-ACO(1,ID,IP1)-ACO(1,ID,IP1)+BCO(1,ID,IP1)+BCO)
BC2 = BC2+DID*(AC2(1,ID,IP1)-BC2)+DIP*(AC2(1,ID,IP1)+BC2)
BC5 = BC5+DID*(AC5(1,ID,IP1)-BC5)+DIP*(AC5(1,ID,IP1)+BC5)
BC6 = BC6+DID*(AC6(1,ID,IP1)-BC6)+DIP*(AC6(1,ID,IP1)+BC6)
11,ID1,IP1) = BC0+DID*(ACO(1,ID,IP1)-BC0)+DIP*(ACO(1,ID,IP1)-BC0(1,ID,IP1)+BCO)
SHIFT MOMENT CENTER FROM XREF TO C.G.
BCO0 = BCO0-(XS-XREF)*BCO
BC6 = BC6-(XS-XREF)*BC5
HYDROSTATIC AND HYDRODYNAMIC FORCES
FZH(J) = -G*BCO-U*U*A33S*THE TA-U*A33S*W+Q*U*(-BC2+A33S*XSS)-U*A33S
1*P*YLSW
FMH(J) = -U*XSS*XSS*A33S*Q+G*BCO0+U*(A33S*XSS+BC2)*(W+U*THETA+YLSW
1*P)
FYH(J) = -A22S*U*(V+XSS*R-ZS*P)
FNH(J) = FYH(J)*XSS-U*((V-ZS*P)*BC5+R*BC6)

```

C C C

C C C

C

SDWL1300
SDWL1310
SDWL1320
SDWL1330
SDWL1340
SDWL1350
SDWL1360
SDWL1370
SDWL1380
SDWL1390
SDWL1400
SDWL1410
SDWL1420
SDWL1430
SDWL1440
SDWL1450
SDWL1460
SDWL1470
SDWL1480
SDWL1490
SDWL1500
SDWL1510
SDWL1520
SDWL1530
SDWL1540
SDWL1550
SDWL1560
SDWL1570
SDWL1580
SDWL1590
SDWL1600
SDWL1610
SDWL1620
SDWL1630
SDWL1640
SDWL1650
SDWL1660
SDWL1670
SDWL1680
SDWL1690
SDWL1700
SDWL1710
SDWL1720
SDWL1730
SDWL1740
SDWL1750
SDWL1760
SDWL1770

```

C      ADD VERTICAL FORCE DUE TO DEADRISE PROJECTION OF LATERAL FORCE
C
C      CTNDR = 0.0
C      IF (DSS.LE.0.0) GO TO 10
C      CTNDR = (BS-BB(1))/DSS
C      IF (THETA.LT.0.0) CTNDR=.39391
10    CONTINUE
C      FZHDLD(J) = FZH(J)
C      FZHDRP(J) = PM1*FYH(J)*CTNDR*PROMO1
C      FZH(J) = FZH(J)+FZHDRP(J)
C      IF (IMT.EQ.2) GO TO 11
C
C      CALC OF FORCE ON VENTRAL FINS REMOVED
C
11    CONTINUE
C      IF (IMT.EQ.2) GO TO 12
C
C      TOTAL SIDEWALL FORCES AND MOMENTS
C
C      FX = FXH(1)+FXH(2)
C      FY = FYH(1)+FYH(2)
C      FZ = FZH(1)+FZH(2)
C      FK = (FZH(2)-FZH(1))*YSW+FKD-FY*ZS
C      FY = FY+FYD
C      FM = FMH(1)+FMH(2)+ZS*FX
C      FN = FND+FNH(1)+FNH(2)+(FXH(1)-FXH(2))*YSW
C
C      DRAG FORCE ON FINS REMOVED
C
12    CONTINUE
C
C      ADD ROLL DAMPING DUE TO VERTICAL WAVE GENERATION
C
C      DSS = Z+ZS-XSS*THETA
C      ZOR1 = (SIGN(1.,DSS)+1.)/2.
C      DSS = DSS*ZOR1
C      DS = Z+ZS
C      DSP = DS-(XREF-XS)*THETA
C      ID = 1.+(DSP*12.-SDS)/DDS
C      ID = MAXO(MINO(ID,NDS),1)
C      DDSR = (ID-1)*DDS+SDS
C      ID1 = MINO(ID+1,NDS)
C      DID = (DSR*12.-DDSR)/DDS
C      BC2 = AC2(1,ID,IP)
C      BC2 = BC2+DID*(AC2(1,ID1,IP)-BC2)+DIP*(AC2(1,ID,IP1)-BC2+DID*(AC2(1,
C      1,ID1,IP1)-AC2(1,ID,IP1)-AC2(1,ID1,IP)+BC2))
C      FKCLD = FK

```



```

C      FK = FK-PROMO2*YSW*YSW*BC2*P/PI
      FZH(1) = FZH(1)+PROMO2/2.*YSW*BC2*P/PI
      FZH(2) = FZH(2)-PROMO2/2.*YSW*BC2*P/PI
      IF (PROMO3.EQ.1.0) WRITE(6,15) VAL(1),FZHOLD(1),FZHOLD(2),FZHDRP(
11) ,FZHCRP(2),FZH(1),FZH(2),FKOLD,FK
      IF (ISIDWL.NE.ON) RETURN
C      DO 13 I=1,2
C
C      DO 13 J=1,11
      GAP(I,J) = 12.0*GAP(I,J)
13   DSW(I,J) = 12.0*DSW(I,J)
C
C      WRITE (6,16) ((GAP(I,J),J=1,11),I=1,2),((DSW(I,J),J=1,11),I=1,2),F
1X,FY,FZ,FK,FM,FN
C
C      RETURN
C
14   FORMAT (/10X,43HWATER CONTACT WITH TOP OF BUBBLE CHAMBER ATF7.2,14SDWL2450
1H FT. TIME =F7.2,19H SEC. IMMERSION=F7.2,4H FT.)
15   FORMAT (/2X,TIME=,1X,E15.4,2X,OLD VERTICAL FORCES,2(5X,E15.4)/SDWL2470
1 25X,VERTICAL DEADRISE FORCES,2(5X,E15.4)/25X,NEW VERTICAL FORCSDWL2480
2ES,2(5X,E15.4)/25X,OLD AND NEW ROLL MOMENTS,2(5X,E15.4)/SDWL2490
16   FORMAT (/10X,8HSIDEWALL/25H GAP (FT.) (STERN TO BOW)/14H PORT SIDE SDWL2500
1WALL/11F10.5/14H STBD SIDEWALL/11F10.5/37H IMMERSION DEPTH (FT.) (SDWL2510
2STERN TO BOW)/14H PORT SIDEWALL/11F10.5/14H STBD SIDEWALL/11F10.5/SDWL2520
310X,26FSIDEWALL FX,FY,FZ,FK,FM,FN/6F15.4)
      END
C
C      FUNCTION SHXYAX (X,Z,ANGYAX,PI)
C
      H = SQRT(X*X+Z*Z)
      IF (X.EQ.0.0) GO TO 1
      ARG = Z/X
      ANGOLD = ATAN(ARG)
      IF (ANGOLD.GE.0.0) GO TO 2
      ANGNEW = ANGOLD+PI-ANGYAX
      GO TO 3
1     ANGNEW = PI*.50-ANGYAX
      GO TO 3
2     ANGNEW = ANGOLD-ANGYAX
3     SHXYAX = H*COS(ANGNEW)
C
      RETURN
      END
      SUBROUTINE STNSL
      SSL 10

```



```

C      ELSKIL(J) = 0.0
C      AIRLEN(J) = 0.0
C      1 CONTINUE
C
C      *EFDEP* IS THE EFFECTIVE LIFTING DEPTH OF THE STERN SEAL
C
C      EFDEP = 6.0
C      MM = EFDEP
C      ALSS = 0.0
C      FX = 0.0
C      FZ = 0.0
C      FK = 0.0
C      FM = 0.0
C      FN = 0.0
C      AGAP1 = 0.0
C      AGAP2 = 0.0
C      AGAPA1 = 0.0
C      DELP = PSS-PB
C      IF (DELP.LT.0.0) DELP=0.0
C      PBAR = PB-PINF
C
C      CALCULATE ELSKI HERE.
C
C      SINDIF = SINTH-COSTH*THETA
C      COSDIF = COSTH+SINTH*THETA
C      X1 = XSS+ZSS*THETA-XLF*SINDIF
C      Z1 = (-Z-ZSS+XSS*THETA-ELMAXS*COS( THETA))
C
C      CALCULATE GAP HERE.
C
C      N = NSTA(4)
C
C      DO 2 K=1,N
C        ELSKI(K) = (ETA(4,K)-DETADX(K)*(XX(4,K)-X1)-Z1)+YY(4,K)*PHI-XPWV*W
C          1ATSLP
C        IF (ELSKI(K).GT.HINGHT) ELSKI(K)=HINGHT
C        ELSKIL(K) = ELSKI(K)+GPS
C        IF (ELSKIL(K).GT.HINGHT) ELSKIL(K)=HINGHT
C        IF (ELSKIL(K).LT.(HINGHT-ELMAXS)) ELSKIL(K)=HINGHT-ELMAXS
C        GAP(K) = -ELSKI(K)+(HINGHT-ELMAXS)
C        IF (GAP(K).LT.0.0) GAP(K)=0.0
C        MM1 = ELSKIL(K)*12.0
C        MM2 = MM1+1
C        MM3 = MM2+1
C        DLINC = ELSKIL(K)*12.0-MM1
C        STNSL1 = CTNSL(MM,MM2)
C        STNSL2 = CTNSL(MM,MM3)

```

```

C      AIRLEN(K) = ((STNSL2-STNSL1)*DLINC+STNSL1)/12.0
2 CCNTINUE
C
C      N = NSTA(4)-1
DO 5 J=1,N
  ELSKIA = (ELSKIL(J+1)+ELSKI(J))*0.5
  ELSKLA = (ELSKIL(J+1)+ELSKIL(J))*0.5
  AIRLAV = (AIRLEN(J+1)+AIRLEN(J))*0.5
  AGAP = ELSKIA-ELSKIA
  AGAP1 = AGAP
  IF (AGAP.LT.GPS) AGAP=GPS
  IF (AGAP1.GT.GPS) AGAP1=GPS
  ARMIS(J) = XX(4,J)+ELSKIA*0.5
  ARM2S(J) = ZS-ELSKIA
  DFSS(J) = -DELP*DELYSS*AIRLAV/(GPS/AGAP)**2
  IF (AIRLAV.LE.0.0) GO TO 3
  ARG = .5*RHO*U*AIRLAV*DELYSS
  RESKI = U*AIRLAV/ENJ
  CDTSKI = .427/(ALOG10(RESKI)-.407)**2.64
  TSKIS(J) = -ARG*CDTSKI
C
C      THE FOLLOWING CARD REMOVES WATER DRAG EFFECTS OF STERN SEAL
C
C      TSKIS(J) = 0.0
C      GO TO 4
3 TSKIS(J) = 0.0
4 CONTINUE
  FX = FX+TSKIS(J)
  FZ = FZ+DFSS(J)
  FK = FK+DFSS(J)*YAVGS(J)+TSKIS(J)*ARM2S(J)
  FM = FM-DFSS(J)*ARMIS(J)*YAVGS(J)
  FN = FN-TSKIS(J)*YAVGS(J)
  ALSS = ALSS+(GAP(J)+GAP(J+1))*DELYSS*0.5
  AGAP2 = AGAP+AGAP1
  AGAP1 = AGAP2/J
5 CONTINUE
C
  ALSS = ALSS+ALEAK*(AGAP1/GPS)
  SQFAC = SQRT(2.*ABS(PBAR)/RHOINF)
  QL = CFSS*ALSS*SQFAC*SIGN(1.,PBAR)
  IF (ISTNSL.NE.ON) RETURN
  WRITE (6,6) GAP,AIRLEN,FX,FY,FZ,FK,FM,FN
C
C      RETURN
C
6 FORMAT (//12H STERN SEAL/26H GAP (FT.) PORT TO STBD. /11E11.3/28SS

```


WAVS 750
WAVS 760
WAVS 770
WAVS 780
WAVS 790
WAVS 800
WAVS 810
WAVS 820
WAVS 830
WAVS 840
WAVS 850
WAVS 860
WAVS 870
WAVS 880
WAVS 890
WAVS 900
WAVS 910
WAVS 920
WAVS 930
WAVS 940
WAVS 950
WAVS 960
WAVS 970
WAVS 980
WAVS 990
WAVS 1000
WAVS 1010
WAVS 1020
WAVS 1030
WAVS 1040
WAVS 1050
WAVS 1060
WAVS 1070
WAVS 1080
WAVS 1090
WAVS 1100
WAVS 1110
WAVS 1120
WAVS 1130
WAVS 1140
WAVS 1150
WAVS 1160
WAVS 1170
WAVS 1180
WAVS 1190
WAVS 1200
WAVS 1210
WAVS 1220

```

C      FMW(J) = 0.0
      FNW(J) = 0.0
      4 CCNTINUE

C      XSS = -XS
      IF (IMT.EQ.2) XSS = XMI(IX)
      IP = 1+(THEBAR*RAD-STH)/DTH
      IP1 = MAXO(MINO(IP,NTH),1)
      IP1 = MINO(IP+1,NTH)
      DTHETA = (IP-1)*DTH+STH
      DIP = (THETA*RAD-DTHETA)/DTH
      TIME RISE FACTOR FOR WAVE AMPLITUDE
      AMPFAC = 1.-EXP(-TIME/AMPTC)

C      DO 11 I=1,NWAVE
      CM1 = CMEGA(I)
      CM2 = CM1*CM1
      XWK = CM2/G
      AA = AW(I)*AMPFAC
      FT = CM1*TIME+XWK*F0
      AL = XWK*COGAM
      IAA = 1+(ABS(AL)-SAL)/DAL
      IAA = MAXO(MINO(IAA,NAL),1)
      IAA1 = MINO(IAA+1,NAL)
      DAA = (IAA-1)*DAL+SAL
      DIA = (ABS(AL)-DAA)/DAL
      SALP = SIGN(1.,AL)

C      WAVE FORCES AND MOMENTS ON THE SIDEWALLS

C      DO 7 J=1,2
      YLSW = (2#J-3)*YSW
      WE = FT+XWK*SIGAM*YLSW
      ST = SIN(WE)
      CT = COS(WE)
      DSR = ZBAR+ZS+YLSW*PHIBAR
      ID = 1.+(DSR*12.-SDS)/DDS
      ID = MAXO(MINO(ID,NDS),1)
      DDSR = (ID-1)*DDS+SDS
      CID = (DSR*12.-DDSR)/DDS
      ID1 = MINO(ID+1,NDS)
      DSS = DS-XSS*THEBAR
      ZOR1 = (SIGN(1.,DSS)+1.)*0.5
      DSS = DSS*ZOR1
      IDSS = 1.5+(DSS-SBB)/DBB
      IDSS = MINO(NBB,IDSS)

```


C
C
C

SHIFT MCMENT CENTER FROM XREF TO C.G.

BC00 = BCC0-(XS-XREF)*BC0
BC3 = BC3-(XS-XREF)*BC1
BC4 = BC4-(XS-XREF)*BC2
BC6 = BC6-(XS-XREF)*BC5
BS00 = BS00-(XS-XREF)*BS0
BS3 = BS3-(XS-XREF)*BS1
BS4 = BS4-(XS-XREF)*BS2
BS6 = BS6-(XS-XREF)*BS5

C
C
C

CALCULATE WAVE FORCES AND MOMENTS

FZC = BS1-XWK*G*(BS2+BS0)-U*OM1*(-A33S*CK-AL*BS2)
FZS = BC1-XWK*G*(BC2+BC0)+U*OM1*(-A33S*SK+AL*BC2)
FMC = BS3-XWK*G*(BS4+BS0)-U*OM1*(-A33S*CK-BC2-AL*BS4)
FMS = BC3-XWK*G*(BC4+BC0)+U*OM1*(-A33S*SK-BS2+AL*BC4)
FYS = XWK*G*(BC5+BC0)-U*OM1*(-A33S*SK+AL*BC5)
FNC = -XWK*G*(BS5+BS0)-U*OM1*(-A22S*CK-AL*BS5)
FNS = XWK*G*(BC6+BC0)-U*OM1*(-A22S*SK-BS5+AL*BC6)
FCS = -XWK*G*(BS6+BS0)-U*OM1*(-A22S*CK-BC5-AL*BS6)
FKS = XWK*G*(BC7-BC8)+U*OM1*(-A42S*CK+AL*BC8)
FKS = -XWK*G*(BS7-BS8)+U*OM1*(-A42S*CK-AL*BS8)
FZW(J) = FZW(J)-AA*(FZC*CT+FZS*ST)
FZW(J) = FMW(J)+AA*(FMC*CT+FMS*ST) *SIGAM
FZW(J) = FYW(J)-AA*(FYS*CT+FNS*ST) *SIGAM
FZW(J) = FNW(J)-AA*(FNC*CT+FKS*ST) *SIGAM
FZW(J) = FKW(J)-AA*(FKC*CT+FKS*ST) *SIGAM
FZW(J) = FXW(J)-2.*AA*RHO*G*BS*DS*SK*CT

7

IF (IMT.EQ.2) GO TO 11

WAVE ELEVATION AROUND THE SIDEWALLS AND SEALS

DO 8 J=1,4
N = NSTA(J)

DO 8 K=1,N
ETA(J,K) = ETA(J,K)+SIN(XWK*(-XX(J,K)*COGAM-YY(J,K)*SIGAM)+FT)*AA
CONTINUE

8

ETACG = ETACG+AA*SIN(FT)
N = NSTA(3)

DO 9 J=1,N

WAVS 2190
WAVS 2200
WAVS 2210
WAVS 2220
WAVS 2230
WAVS 2240
WAVS 2250
WAVS 2260
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WAVS 2660

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